

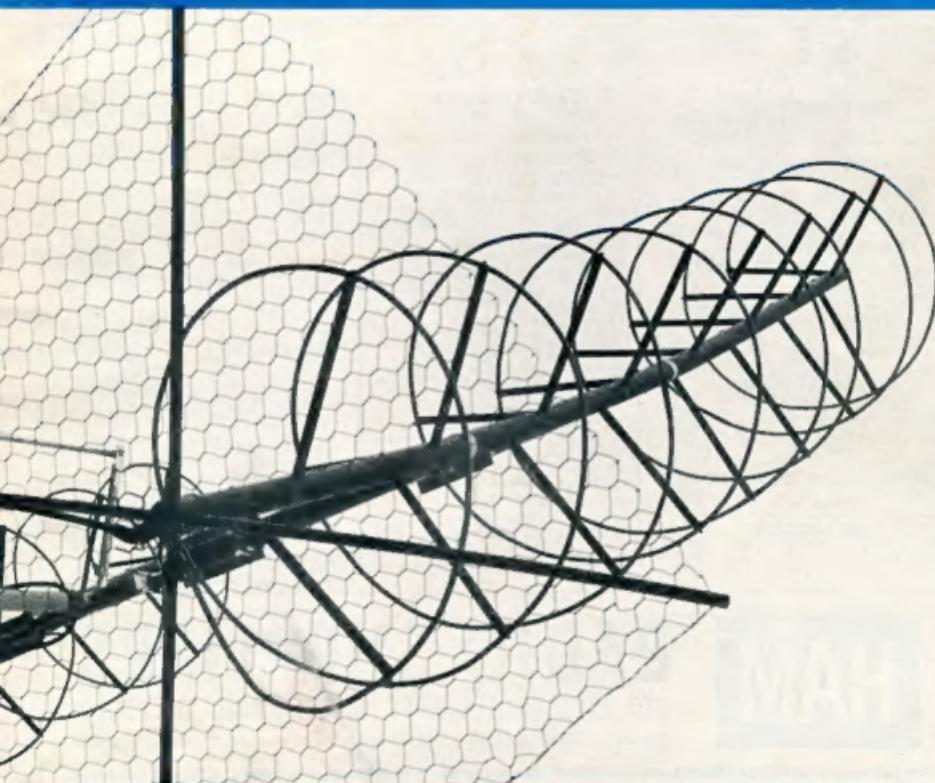
amateur radio

JOURNAL OF THE WIRELESS INSTITUTE OF AUSTRALIA

NOVEMBER, 1972

Registered at G.P.O., Melbourne, for
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Category 'B'

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Specifications: 0-300, 250, 500, 2500.

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Capacity: 0.01-0.3 uF (at A.C. 5v.); 0.0001-0.01 uF (at A.C. 50v.).

Output voltage: 0.5v., 1.5v., 2.5v., 5v.

Battery: 9V, UM3, 1.5v., 1-piece.

Dimensions: 3 1/2 x 1 1/2 x 1 1/2 inches.

With internal battery, probe, leads, probe.



MODEL AS-1000/P

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AC volts: 6, 30, 120, 300, 600, 1000, 10K (s.p.d.v.).

DC current: 12, 100, 500, 1000, 10K (s.p.d.v.).

0.001-0.1 ohms. DC current: 12 mA, 8 mA, 5 mA, 3mA, 1.5mA.

Resistance (ohms): 2K, 200K, 4K, 400K, 4mA, 40 megohms.

dB scale: minus 20 to plus 63 dB. Audio output (voltage AC): 5, 30, 120, 300, 500 dB.

Battery: Internal. Approx. size: 7 1/2 x 8 1/2 x 2 1/2 inches.

MODEL OL-64D

Price \$16.75

20,000 ohms per volt. DC voltage: 0.025, 1, 10, 50, 250, 500, 1000 (20K o.p.v.). 3000 (30K o.p.v.).

AC voltage: 10, 50, 250, 500, 1000, 10K (s.p.d.v.).

DC current: 12, 100, 500, 1000, 10K (s.p.d.v.).

0.001-0.1 ohms. Resistance (ohms): 100K, 10K, 1000, 100, 10, 1 ohm.

Inductance (ohms): 4K, 400K, 4mA, 40 megohms.

dB scale: minus 20 to plus 38 dB. Capacitance: 250 pF to 0.02 uF. Inductance: 0.5000 Henries.

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0.001-0.1 ohms. Resistance (ohms): 100K, 10K, 1000, 100, 10, 1 ohm.

Inductance (ohms): 12K, 120K, 1.2M, 12M, 120M, 1200M.

dB scale: minus 20 to plus 62 dB. Approx. size: 5 1/2 x 3 1/2 x 1 1/2 inches.

MODEL 10/A/P

Price \$55.00

Overall dimensions: 4 1/2 x 2 1/2 x 1 1/2 inches.

AC voltage: 2.5, 10, 50, 250, 500, 1000 (10K o.p.v.).

DC voltage: 0.5, 2.5, 10, 50, 250, 500, 1000 (10K o.p.v.).

DC current: 0.5, 2.5, 10, 50, 250, 500, 1000 (10K o.p.v.).

0.001-0.1 ohms. Resistance (ohms): 100K, 10K, 1000, 100, 10, 1 ohm.

Inductance (ohms): 100K, 10K, 1000, 100, 10, 1 ohm.

Capacitance (uF): 2.5, 10, 50, 250, 500, 1000 (10K o.p.v.).

Resistance (ohms): 100K, 10K, 1000, 100, 10, 1 ohm.

dB scale: minus 20 to plus 62 dB. Signal injector: Blocking oscillator circuit with a 2SA102 transistor. Approx. size: 6 1/2 x 7 1/4 x 3 3/4 inches.



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amateur radio

JOURNAL OF THE WIRELESS INSTITUTE OF AUSTRALIA. FOUNDED 1910



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CONTENTS

	Page
TECHNICAL—	
Satellite Track Calculator	3
AO-C 2 Metre to 10 Metre Repeater	5
The Amsat Oscar-C Command System	7
The Amsat Oscar-C Telemetry System	10
A Solid State Electronic Keyer	13
An Integrated Circuit I.F. Strip	15
Newcomer's Notebook	16
Commercial Kinks:	
Conversion of A.W.A. F.M. Carphones, Part 2	17
The Trio 9R 59DE/DS	17
After Thoughts—on an F.M. Repeater	17
DEPARTMENTS—	
Intruder Watch	24
Ionospheric Predictions	23
Key Section	23
Letters to the Editor	24
Magazine Index	23
New Call Signs	21
OSP	2
VHF UHF: an expanding World	21
You and DX	20
"20 Years Ago"	24
GENERAL—	
P.M.G. Examination Papers, August 1972	18
Silent Key	24
CONTESTS AND AWARDS—	
Awards Column	18
Contests—R.D. Contest to VK5	19
Corrections to VK-ZL 1972 Contest Results	16
COVER	
Portion of the twin helix 2 metre satellite tracking array used by VK3ABP. The helices are 12 ft. long of eight turns of 3/8 in. aluminium tubing, and the array is remotely controllable in elevation and azimuth.	
Photo: VK3YAZ and VK3ZU.	
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At page 15 of the August issue of "A.R." we reported on the results of the special Conference held at Albury on 8th and 9th July, 1972, to consider the possible alteration of existing repeater and simplex channels in the 2 metre band.

The Conference arose from proposals put forward by the Victorian Division with a view to leaving the allocation 144 to 146 MHz. clear for Satellite operation, that being the segment allocated for that purpose as a result of the 1971 W.R.A.C. on Space Communications.

The recommendations of the Conference were circulated as a postal vote for Federal Council. The Executive delayed the circulation of this postal vote for some time to enable full discussion of the proposals to take place at Divisional and other meetings. In fact the proposals have generated some intense debate and many Amateurs interested in this area of operation have formed extremely strong views either for or against the proposals to alter the existing channels.

It is interesting to record that in a matter of days before the circulation of the postal vote the Federal Communications Commission released a report and order prohibiting terrestrial repeaters in the U.S.A. between 144 and 146 MHz. to preserve for satellite communications the world-wide band from 144 to 146 MHz. (the band 144-148 MHz. is allocated to the Amateur Service **only** in Regions 2 and 3).

1973 CALL BOOK

All members of the Publications Committee have been working very hard during the past few months to improve "A.R." and with the able help of the Contributing Editors, Drafting Assistants, and Publishing Associates, we feel that, within the stringent economic limitations imposed upon us, we are gradually improving the presentation and content of the magazine. And, most important, the financial situation is looking better all the time.

One of the duties of the Publications Committee is the production of the Call Book. The preliminary planning and costing of the 1973 Call Book has been completed, and I am sure that all Amateurs will be pleased with the improved format, the additional information, and the cost of the finished article.

However, the most important part of the Call Book, the station listings, is causing considerable concern.

At the closing date for this Call Book, 31st December, 1972, the P.M.G. Dept. will provide us with the official lists of all Amateur Stations under the control of the Australian administration. We will then check against our own index system, which are continually updated from news items in "A.R.", as well as from written forms of advice we receive from Amateurs themselves.

So, you say, what is the problem?

Simply this. A rough check on our index system against the mailing list for "A.R." shows that a large number of Amateurs are receiving the magazine at an address different from their station address.

Does this mean that they now have a separate post office box for their station address or does it mean that the station address has also changed? We don't know!

Unless the change-of-address advice received by us is reliable, then the only course is to use the new station address, and is not just a new address for "A.R." we are unable either to alter the Call Book index or to advise the P.M.G.

If your mailing address, as shown on your "A.R." wrapper, is **NOT** also your station address, please let us know as soon as possible and give us your full station address. This is needed only if your 1971 Call Book details have changed or are incorrect.

Are you blameless of this type of change-of-address advice?

If your address was incorrect in the last Call Book, or has changed since the last issue, and you are not able to assure that you advised both the W.L.A. and the P.M.G. in the correct manner, please do something about it NOW.

If you want to be correctly listed in the 1973 Call Book, you **MUST** advise us at least of any amendment, and the P.M.G. Dept. will then advise the P.M.G. Dept. of the alteration, and the official lists as printed in the 1973 Call Book should be as accurate as you can make them.

—Call Book Sub-Committee.

OTHER SERVICES

The charges for obtaining television programmes via satellite (Invisat) remain at \$650 for the first ten minutes and \$40 for each additional minute. (Aust. Br. Control Board, 24th Annual Report.)

CALL SIGN BLOCKS

The L.T.U. has allocated to Open (Sulmanite) the call sign block A4A to A4Z, and to Bangladesh the block S2A to S2Z. (Reg. I News.)

ITALIAN LICENSING

In Italy it appears there are four classes of licence available, but mobile operations are not permitted. The class 1 licence allows up to 75W input on v.h.f. and up to class 3 up to 350W and a new technician's licence (theory exam only) for 10W. input on v.h.f. and u.h.f. bands only. (I.A.R.U. Reg. I News.)

TRANSISTORS AND VALVES

The percentage of total usage of transistors and valves in 1970 was: 10% for valves, 5% transistors, and 1% ICs. For 1972 these were quoted as 30%, 49% and 21% respectively. By 1974 the percentages are expected to be 5%, 35% and 59% respectively. (WALS Bulletin.)

It is also interesting to note that the v.h.f. repeater group in the Southern California area, at a meeting held on 9th September, adopted a frequency allocation plan in that area which will require the voluntary shifting of frequencies by more than 50 repeaters. I do not offer this information in support of the proposals circulated, but draw your attention to them as evidence of a global concern for the problem placed before the Federal Council by the postal vote for their consideration.

The Federal Councillor of the New South Wales Division, Mr. Don Miller, VK2GN, has given notice in accordance with Article 44 of the Institute's Articles of Association that he requires the matters the subject of this postal poll to be held over for determination at the next Federal Convention. The right to take this step in relation to a postal poll of the Federal Council is given to each Federal Councillor. The object of this Article is to provide a means of protection against hasty decisions on important matters without the opportunity for adequate discussion.

Accordingly, the Federal Council is unable to determine the matter by a postal poll and the Institute will not adopt at this time, nor can it adopt prior to the Federal Convention any policy seeking the change of the existing repeater allocations. Whether the Council will decide to preserve the status quo or adopt a new policy will be decided by the Federal Council at the next Federal Convention.

MICHAEL J. OWEN, VK3KL
Federal President, W.I.A.

SWITZERLAND

Licensing authorities are now prepared to allow repeaters having input and output frequencies in the 2 metre band. It is not expected that many amateur repeaters will be installed, since five repeaters are now operating in the 70 cm. band, giving excellent results. The latter band proves to be superior for mobile work in cities and mountainous areas. (I.A.R.U. Reg. I News, Aug. '72.)

MARCO

Marco means "Medical Amateur Radio Council". In a recent letter JA0BXP/1, C/o Nomura 2-21-9 Ogikubo, Suginami-ku, Tokyo 167, writes that he is Marco correspondent in Japan but is hampered by the absence of an Asia-Oceania section to prepare for any medical amateur section. If you are a Radio Amateur Medical Practitioner, you might care to write to him direct to set up such.

PORTABLE AND MOBILE OPERATIONS

A recent letter from the Director-General P.M.G.'s Department Radio Branch (RB1/17/46) clarifies the meaning of paragraphs 80 and 81 in the Handbook. The letter states, inter alia, "portable and mobile operations are limited to in these paragraphs including the 'five consecutive days' when no approval is required, means absences of a licensed Amateur from his fixed station address during which he is in possession of portable or mobile equipment capable of being used in the Amateur Service".

In further elucidation, it has been ascertained that the key to the situation is "absence from the fixed station address".

If you do NOT go away from your fixed station address for more than five days at any one time you can, of course, work portable or mobile equipment approved by the P.M.G. If you are away from your fixed station address for more than five days at any one time and you take with you, or use, portable or mobile equipment in that period you must obtain special approval to operate portable or mobile even if only for a few minutes.

BARNS

If your signal puts some across your neighbour's tv, you could go out into too many, come out singing a few, and end up behind some—even if you are a sheep farmer.

SATELLITE TRACK CALCULATOR

P. D. FRITH,* VK7PF

In this article VK7PF describes what is possibly one of the simplest ways yet devised of making orbital predictions for a satellite such as Amsat Oscar-C. He also gives some sound practical advice on antenna pointing while attempting communication through the satellite translator.

This visual method plots the path across the earth of a satellite and from this determines:

- (1) In what direction will it first be heard and at what time (acquisition of signal, or a.o.s.).
- (2) The bearing, time and elevation at closest approach (t.c.a.).
- (3) The loss of signal (l.o.s.), direction and time.

For communication purposes it is required to know areas of possible contacts. These can be found by using overlays for the particular areas and establishing whether there is a common overlap period when the satellite is within range of both stations.

SOME TERMS

Before going into details, some terms used in tracking satellites will be given and explained. When the first Oscars were tracked I had difficulty in finding a suitable text to explain in just the right amount of detail the mechanism of how and why a satellite orbits where it does and Ref. 1 is to be recommended as that text.

Orbit.—A satellite is in orbit when it revolves around the earth in a plane which passes through the earth's centre. This means that it has to spend time in both the north and south hemispheres. It is not possible to orbit around say 40°S latitude only.

Orbit Number.—The start of an orbit is said to be when a satellite passes over the equator on a north bound track (ascending node) and the number of the orbit changes at that time. It will be seen from the calculator that it also passes over the equator south-bound (descending node) approximately 180° further west.

Inclination.—This is the angle the plane of revolution makes with the equator at the start of an orbit with east as reference. For AO-C this will be 102°, which is the angle required for the chosen height to cancel the influences that would move the daily viewing time away from the chosen 9 o'clock local sun time.

Progression of Tracks.—The plane of the orbit in which the satellite revolves can be regarded as fixed with the earth rotating beneath. This means that successive equator crossings in the same direction will be further to the west and because of this the longitude scale on the equator is marked in degrees west only.

Period.—The time of one revolution. For earlier Oscars this varied but the changes will be of no consequence for AO-C.

Predictions.—These are usually given as orbit numbers, the time of the start of this orbit (as it crosses the equator northbound) and the west longitude of this crossing.

THE CALCULATOR

This takes the form of a polar map, that is, a great circle map with the south pole as centre. Two sample tracks are shown on Fig. 1, one south-bound east of Australia and the other north-bound in the same area. The first would be around 8 a.m. and the other around 9 p.m. The tracks are actually great circle paths corrected for the earth's rotation as the satellite moves along them. The north-bound track crosses the equator south-bound at 006.5°W, passes to the east of the pole and northwards to cross the equator at 200.5°W (006.5 + 180 + 14.4) and into the next orbit.

The south-bound track crosses the equator seven orbits later at 207.5°W,

passes to the west of the pole and then north-wards to cross the equator at 41.0°W (207.5 + 180 + 14.4 = 380). The earth rotates 14.4° during half an orbit or 28.8° for a full orbit of AO-C (115 min. period).

The next N-S crossing will be at 236.3°W.

Shown in Fig. 2 are two sample range diagrams which have to be used for the particular latitude of interest. The ones supplied with the tracking kit, being made available, will be for most latitudes and be on transparent paper.

USING THE CALCULATOR

Select the range ring for your latitude and fix it over the map with the centre at your location, or better still, copy it onto the map to leave the transparency free for use at other locations. Fix the map onto a baseboard of heavy cardboard or other suitable material and the AO-C track onto a piece of perspex. Pivot by some means the perspex with the indicated south pole at the south pole of the map. Now you can do a trial run of a typical day's

(continued on page 13)

Fig. 1

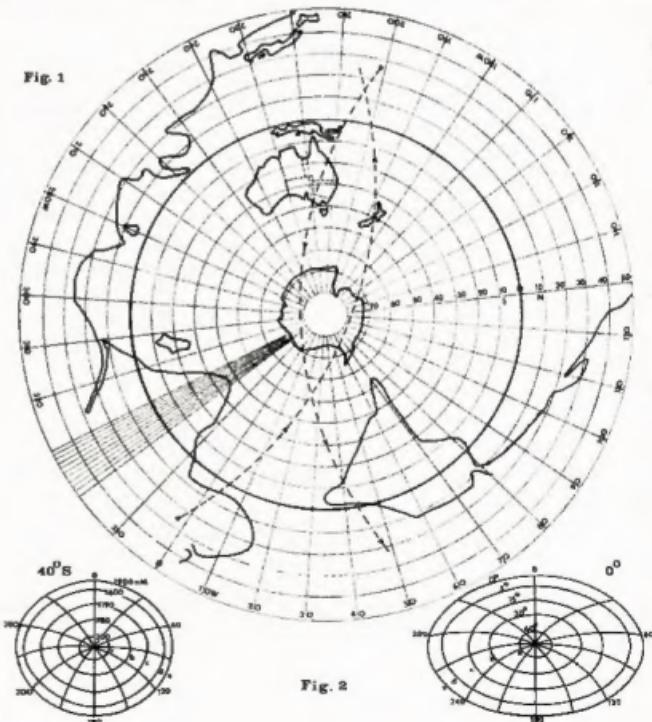


Fig. 2

SIDEBOARD ELECTRONICS ENGINEERING

BARGAINS!!

YAESU MUSEN FTDX560 Transceivers, 500W. PEP	\$520
FTDX401 = FTDX570 plus CW filter	\$580
MOSLEY TA33JR Junior Triband Beam	\$95
Mustang MP33 1kw. Triband Beam	\$115
HY-GAIN TH3JR Junior Triband Beam	\$110
CDR ROTATORS with 220v. indicator/control units:	
AR22-R	\$40
Hem-M	\$130
FRONTIER Digital 500 500W. PEP Transceiver	\$400
FT241A CRYSTALS , 375-515 kHz., per box of 80 crystals 1854 Hz. apart, per box one 400, 455 and 500 kHz. rock	\$10
Ex R.A.A.F. Radar Tower, 110 ft. ten-section square aluminium telescoping crank-up with stainless steel guy cables	\$450
Several used but perfect 20-40 M. Duo-Bander Yagis. Also 20 metre traps to build them per pair	\$25
TUBES : 6KD6 or 6JS6A	\$5
6LQ6 or 6HF5	\$6
Still some NATIONAL transformers and chokes left.	

All prices again net, cash with orders, S.T. included. Freight or postage and insurance are extras.

MIDLAND PRODUCTS:	
One-watt Walkie-Talkies with nickel cadmium battery	\$40
Five-watt base-mobile station Transceivers, 240 V. AC or 12 V. DC, with PTT microphone and facilities for eight crystal controlled channels 27-28 MHz., few left	\$70
PTT Dynamic hand-held Microphones	\$10
PTT Dynamic Desk Microphones	\$12.50
PTT Dynamic Desk Mikes with built-in two-stage pre-amplifier	\$17.50
Twin Meter SWR Meters, forward and reflected power readings, 52 ohms	\$20
8 ohm lightweight Headphones	\$5
Crystals for 28.1, 28.2, 28.3, 28.4, 28.5 MHz. channel operation	\$2
Crystals for 27.24, 27.88, 27.125, 27.065, 27.085 MHz. operation	\$3
Midland Crystal pairs on frequencies as stated for transmit and receive 455 kHz. lower in frequency.	

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BOOKS OF INTEREST FOR AMATEUR OPERATORS

● G.E.—SCR MANUAL, including Triacs and other Thyristors—Fifth Edition	\$5.00 posted
● DOVER—BASIC ELECTRICITY	\$4.60 posted
● HEY—A BEGINNER'S GUIDE TO HI-FI	\$1.45 posted
● ORR—VHF HANDBOOK	\$5.75 posted
● SAMS—TRANSISTOR SUBSTITUTION HANDBOOK, No. 11	\$3.10 posted
● SAMS—TUBE SUBSTITUTION HANDBOOK, No. 15	\$2.75 posted
● ORR—BEAM ANTENNA HANDBOOK—New 4th Edition	\$6.85 posted
● R.S.G.B.—AMATEUR RADIO CIRCUITS BOOK	\$2.70 posted
● KING—COLOUR TELEVISION SERVICING	\$15.20 posted
● DAVEY—FUN WITH TRANSISTORS	\$3.65 posted

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AO-C 2 METRE TO 10 METRE REPEATER

G. N. LONG,* VK3YDB
Chairman, Project Australis Group

INTRODUCTION

This article is intended to deal with the operation and design of the Amsat 2 metre to 10 metre linear repeater (translator or transponder).

As an insight into its development here is a short history of the device:

- (a) Designed by Carl Meinzer, DJ-4ZC, in late 1970. The first prototype was built in the autumn of 1971. (This is the one now here in Australia.)
- (b) A second prototype was built in the Spring of 1971 by Mr. P. Klein, K3JTE.
- (c) The flight model for AO-C was built in 1972 by Jan King, Perry Klein and other members of the Amsat organisation.

The launch of the AO-C will bring to the Amateurs of the world a means to find some answers to complex questions about propagation, orbital geometry, and electronic reliability. This is the first satellite in the history of Amateur Radio which contains its own primary power generating source, and it will therefore be a long life system.

It is felt that if the system is "go" ten minutes after launch, then it will work for a year, thus giving us Amateurs an invaluable tool with which to demonstrate to various Administrations around the world that Amateur operators are a valuable asset, not a liability as presently thought by some Administrations.

This satellite has the following uses:

- (a) Education—by Y.R.C.S., school clubs and universities.
- (b) To be available for scientific research by people such as moon-bounce groups, C.S.I.R.O., P.M.G. if they so desire—and by medical groups, interested in remote medical sensing.
- (c) For outback communication, in Central Australia, as an example.
- (d) Further development of small low-cost ground terminals.

These are all great hopes to be fulfilled. The Australian Amateur has done much to help this and, we hope, also the future satellites. To this end we feel that all Amateurs should make maximum use of the **bird**.

Now for a technical description as taken from the latest Amsat Newsletter (September 1972).

THE REPEATER DESIGN

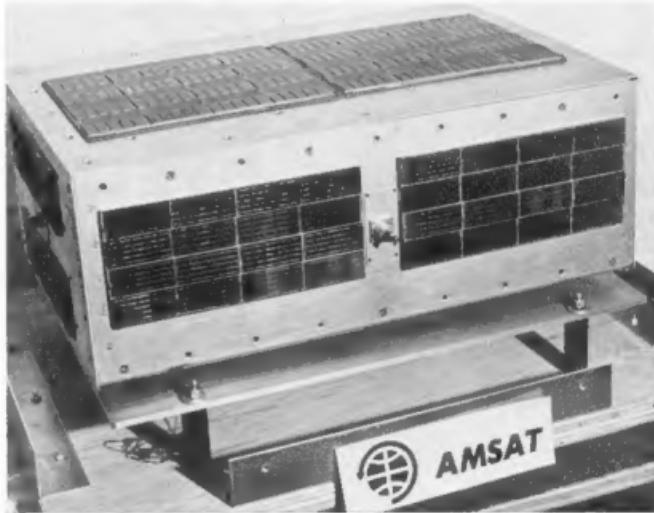
The repeater uses a 2N3478 r.f. transistor as a two metre pre-amplifier and another 2N3478 as the first mixer to mix the two metre received signal down to 39.1 MHz. A 35.61625 MHz. crystal oscillator output is multiplied by three to 106.84875 MHz. and is mixed with the amplified two metre signal to provide this 39.1 MHz. first i.f. fre-

quency. The signal is then fed to a 2N918 second mixer, which uses the 35.61625 MHz. crystal oscillator a second time to mix down to a second i.f. frequency of 3.485 MHz., providing a gain of approximately 20 dB. in the process.

The 3.485 MHz. i.f. signal is then amplified approximately 35 dB. in a single BF167 i.f. amplifier stage, after which it is up-converted to a frequency of 29.5 MHz. in a 2N918 balanced mixer, using a 2N918 crystal local oscillator operating at 26.015 MHz. The balanced

USING THE REPEATER

The repeater is designed for linear operation and is capable of handling most forms of narrowband modulation, s.s.b., c.w., a.m., f.m., r.t.t.y. and s.s.t.v. S.s.b. and c.w. are recommended primary modes of operation and make most efficient use of the repeater because a number of users can operate simultaneously, each taking different proportions of the repeater's power capability at a particular instant of time. Therefore, a higher average power level is available to each user



Photograph of the Amsat Oscar-C (Oscar 6) satellite package, courtesy of Dr. Perry Klein, K3JTE.

mixer achieves a gain of nearly 25 dB., and the signal level at this point is of the order of one milliwatt at 29.5 MHz. The signal is then amplified to a maximum of about 1 to 1.3 watts output using a 2N3868 driver and 2N3375 final amplifier. A.g.c. voltage is developed in a three-transistor a.g.c. amplifier, which senses the emitter current of the final amplifier and controls the gain of the BF167 i.f. amplifier.

The repeater also contains a beacon oscillator which operates at 29.45 MHz., the same frequency used by the last satellite, Australis-Oscar 5. The beacon signal is injected at the input to the driver stage, and the beacon is keyed by the Morse code telemetry encoder or the code-store message storage unit, which are selected alternately at approximately 14 to 15-minute intervals by a clock timer device in the satellite.

since not all c.w. users are key-down at any given instant, nor are all sideband stations talking up to full power at any one moment. A.m., f.m. and r.t.t.y. do not have this characteristic. Thus, stations employing these modes will each expend the available repeater power at all times, even when no intelligence is being transmitted.

To facilitate the most efficient operation of the repeater, all users are strongly urged to continuously monitor their own downlink signals. This is an operating technique previously rarely available to Amateurs, but which enables each user to hear his own signal from the satellite as others hear it. It requires simply that a separate receiver and antenna be available for receiving one's own downlink signal on ten meters, while transmitting simultaneously on the two metre uplink band.

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Such operation makes possible perfect break-in QSOs and roundtables, particularly on s.s.b., permitting full duplex operation.

Unlike other forms of Amateur communications, satellite communications with downlink self-monitoring permits each user to observe how the DX hears his signal, and he can then adjust his power and frequency to compensate for the satellite's distance and Doppler frequency shift. This is most readily done by observing the satellite's beacon signal level on 29.45 MHz, and adjusting the power of the ground transmitter so that the repeated signal from the satellite appears to be the same level, either as read on an S meter or as determined aurally. If the transmitter is v.f.o. controlled, its frequency should be constantly adjusted by the operator while transmitting to keep the apparent downlink frequency constant in the presence of changing Doppler shift, which can be as much as ± 4.5 kHz. for an overhead pass.

Spotting one's own downlink carrier is not always easy through the satellite repeater, and it is quite difficult to zero beat another station without careful dial calibration. One excellent method of getting a "frequency spotter" is to obtain a two metre converter having either a 10 or 20 metre output and use it as a satellite repeater simulator in the shack. If the converter uses a 38.666 or 43.333 MHz crystal, replacing with a 38.817 MHz crystal will convert locally generated two metre signals in the 145.9 to 146.0 MHz. uplink band to the correct frequency in the 29.45 to 29.55 MHz. downlink band, so that spotting and zero beating can be accomplished without the signals leaving the shack.

Because of Doppler shifts up to ± 4.5 kHz. which will occur when using the actual satellite repeater, the spotter's frequency will be off by the amount of the Doppler shift. This can easily be corrected for by setting the transmitter frequency several kHz. higher than the spotted frequency near the beginning of a pass, or several kHz. lower than the spotted frequency near the end of a pass.

OPERATING PROCEDURE

The procedure recommended for operating with the Oscar two-to-one repeater is as follows:

(1) When the satellite comes within range, begin listening for the Morse code beacon signal on 29.45 MHz. Be sure to note the signal strength of the beacon signal. Since the beacon is A1 emission, use your b.f.o. to receive it.

(2) Once you have located the beacon on 29.45 MHz., tune up the band and begin looking for signals from the repeater in the 29.45 to 29.55 MHz. range.

(3) When you are ready to transmit, choose a frequency within the 145.90 to 146.00 MHz. uplink band and send a test signal, preferably a string of dots, on this frequency (f_s). Listen for your own signal re-transmitted from the satellite on the corresponding ten metre frequency (f_{rs}), found from the formula:

$$f_{rs} = f_s - 118.45 \text{ MHz.} \pm f_{DOPPLER}$$

where $f_{DOPPLER} = +4.5$ kHz. near the beginning of an overhead pass.
 $= 0$ kHz. at the middle of the pass.
 $= -4.5$ kHz. near the end of an overhead pass.

For example, a signal transmitted on 145.92 MHz. will be re-transmitted on 29.47 MHz. \pm Doppler. This is where you should listen for your signal. If you can hear your own signal, you can be sure that others can hear your signal as well.

(4) Adjust your transmitter power so that on s.s.b. voice peaks or with a slow string of dots the repeated signal is approximately equal to the beacon signal level. This will assure that you take the correct share of the repeater power without overloading the repeater and running down the satellite's battery unnecessarily. Keep in mind that the power will be divided among all stations in the passband. An overly strong station will prevent other Amateurs from simultaneously using the repeater if he does not reduce his power. He will also reduce the overall repeater gain, through a.g.c. action, so that he will not be able to hear weaker stations who may be trying to call him. If you do not have a convenient method for directly controlling your power output, an alternative technique is to aim your antenna away from the satellite.

If you intend to operate with high power or use a large antenna array such that the transmitter output multiplied by the antenna gain is above 80 to 100 watts effective radiated power, then it is suggested that you operate slightly off from the regular passband of 145.90 to 146.00 MHz. The repeater has an "extended passband" feature in its design, that is the ± 10 dB. response is ± 120 kHz. from the centre frequency (the passband is 240 kHz. wide at the 10 dB. down points). Therefore, if higher power stations will transmit between 145.83 and 145.89 MHz. or from 146.01 to 146.07 MHz., their signals will be compensated for by the roll-off of the repeater response, and they will not take more than the correct portion of the repeater power.

One benefit for doing this is simply a reduction in QRM, since only high power stations can operate through the

repeater on these extended frequency segments. Low power stations cannot easily overcome the additional attenuation of the passband roll-off and should operate in the normal repeater passband of 145.90 to 146.00 MHz.

SUMMARY

In summary, listed below are the basic operating characteristics of the AO-C two-to-one metre linear repeater:

Input frequency range: 145.90 to 146.00 MHz. for normal operation. 145.83 to 146.07 MHz. for extended passband operation.

Output frequency range: 29.45 to 29.55 MHz. for normal operation. 29.38 to 29.62 MHz. for extended passband operation. Passband is non-inverting (i.e. upper sideband remains upper sideband and vice versa).

Beacon frequency: 29.45 MHz. (same as Australis-Oscar 5).

Beacon modulation: Morse code (A1 emission).

Repeater bandwidth: 100 kHz. flat; 120 kHz. at 3 dB. down points; 150 kHz. at 6 dB. down points; 240 kHz. at 10 dB. down points.

Operating modes: S.s.b. and c.w. are recommended; a.m., r.t.t.y. and a.s.s.t.v. can also be used but with less efficiency. F.m. is not recommended.

Repeater power output: 1 to 1.3 watts into a half-wave dipole.

Input sensitivity: Approximately -100 dBm. (2 microvolts/m) for full output.

Ground power required: 80 to 100 watts of effective radiated power produces full output from the repeater at a maximum range of 2,000 miles. (An 8 to 10 watt transmitter and 10 dB. of antenna gain, or 80 watt transmitter and omnidirectional antenna should be adequate.)

Intermodulation: 20 dB. down.

A.g.c.: Up to 20 dB. gain reduction; 0.1 second attack time; 2.2 second release time. Designed for highest efficiency with s.s.b.

Ground receiver required: Better than $\frac{1}{2}$ microvolt/m sensitivity for 10 dB. (S+D)/N on 10 metres should be adequate. Dipole antenna can be used, but beam is preferable.

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THE AMSAT OSCAR-C COMMAND SYSTEM

PETER R. HAMMER,* VK3ZPI

The author has been involved, as a member of the Australis satellite design group, in the development of command systems for the AmSAT Oscar B and C satellites. He discusses here the requirements to be met by a command system and some of the techniques employed in these satellites.

There are several requirements which a command system for a satellite should meet. Firstly, it is necessary to have a sufficiently large number of commands so that the various sub-systems on the spacecraft can be adequately controlled. Secondly, the command system must be secure. This means that the presence of noise and interference at the input of the command decoder must not be decoded as a command. Thirdly, the power consumption of the command decoder must be as low as possible, consistent with the previous requirements. Fourthly, the weight of the command decoder must be as small as possible.

The reason for the last two requirements is that, as the spacecraft weight and power budget are limited, it is desirable that the support systems such as command and telemetry involve as little power and weight as possible so as to leave the maximum amount of power and weight for the main experiments (in this case the 2-10 metre translator and 435 MHz. beacon).

Finally, the command decoder must perform reliably for one year in the harsh environment of space as well as surviving the acceleration and vibration caused by the launch vehicle.

We shall now consider two possible command systems.

* 388 Beach Road, Beaumaris, Vic. 3193.

(a) THE FULLY PARALLEL COMMAND SYSTEM

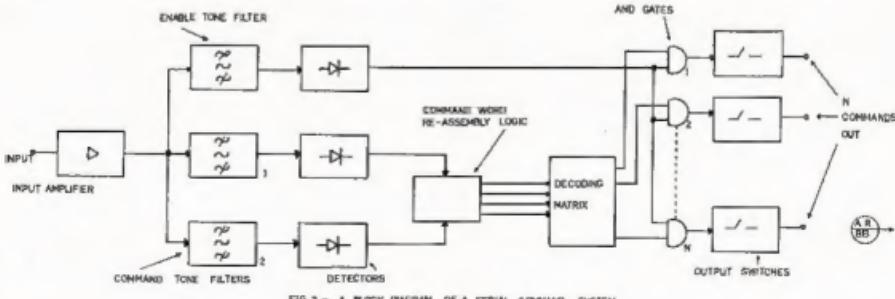
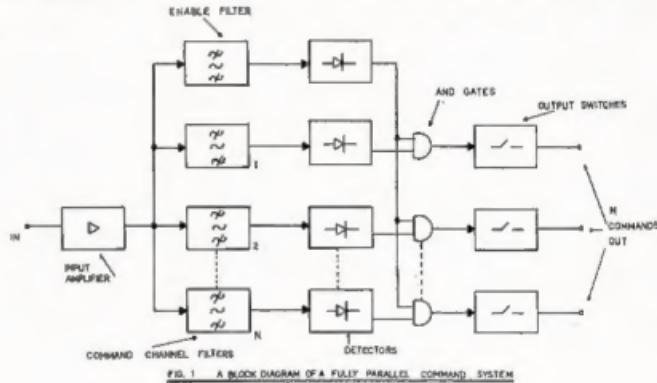
This decoder system is illustrated in Fig. 1. Here we assign each command channel a unique audio tone. When this tone is detected by the decoder, at the decoder input, the appropriate switch at the decoder output is operated. The presence of noise at the decoder input could be interpreted as an erroneous command. To decrease the likelihood of this occurring, we use a separate, unique audio tone, transmitted at the same time as the command tone, to operate an enable gate. Unless this enable tone is present the enable gate is not activated and the decoded command will not be passed through to the output switches.

The decoder scheme described above is very simple and reasonably secure against noise and interference. (Further improvements in this regard can be made by adding additional enable tone systems in parallel with the single one mentioned above.)

The main disadvantage of the fully parallel decoder scheme is that each command needs its own unique tone filter; thus if many command channels are desired the resulting number of filters becomes excessive. The main advantage of the decoder is its inherent redundancy. Provided that the enable channel does not fail, then the failure of one component will only result in the loss of one command. (The enable channel can easily be made redundant, without greatly increasing the weight or the power drain, by duplication of components which are likely to fail.)

(b) THE SERIAL COMMAND SYSTEM

This decoder system is illustrated in Fig. 2. Here we have represented each command by a unique binary word. We transmit the resulting command word in a serial fashion, one bit at a time, and re-assemble the word in the decoder. A decoding matrix in the decoder then decides which command was sent. The decoder for this com-



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mand scheme is thus very similar to a 2-channel parallel decoder; we have replaced the parallel transmission of a large set of possible tones by the serial transmission of a string of two possible tones. (An enable tone can still be used to prevent spurious signals from triggering the decoder.)

In order to correctly re-assemble the bits of the command word it is necessary to have additional information relating to the length of time each bit is sent. This can either be predetermined by the design of the decoder or can be transmitted together with the command word, using a separate timing channel.

The main disadvantage of this decoding scheme is that it is more susceptible to component failure, unless redundancy is designed into each section of the decoder.

It is this latter scheme which has been used for the AO-C spacecraft.

Having decided on the form of the command scheme, we now have to consider how to implement it. Here we are guided by the requirements listed earlier.

The heaviest parts of the decoder are the tone decoding filters. It is possible to use active filters rather than passive filters, but there are two major reasons for not doing this. Firstly, active filters require many more components than passive filters to achieve the same performance and, secondly, the cost and power requirements of the large number of operational amplifiers required is excessive compared to the cost of high quality inductors.

The supply current needed for the analogue portions of the decoder can be minimised by using lower power operational amplifiers and by operating all transistors at very low collector currents. The digital integrated circuits used in the decoder are the only other source of power drain. To minimise this power drain complementary metal-oxide-silicon (COS/MOS) integrated circuits are used. The COS/MOS logic family is based on the use of two series FETs, one P-channel and one N-channel, as shown by the inverter of Fig. 3. As the gates of the two FETs are tied together, only one FET is on at any one time and thus the quiescent

d.c. power drain is due to leakage current through the two series channels. In addition, the output state of the gate is a low impedance at all times and thus the noise immunity of the logic family is very high.

Fig. 4 shows the two circuit boards which comprise the complete 21-channel command decoder for AO-C. (The blank spaces in one board are for additional integrated circuits which can be inserted to give the 35-channel command system intended for AO-B.)

The reliability of the command decoder is greatly determined by the components used and by the construction method. The decoder is built on fibre-glass printed circuit boards which have been solder-coated. Solder coating is preferable to gold plating as the lead in solder forms a brittle amalgam with gold and this can result in a dry joint

protect the system against component failure it is desirable that any redundant commands have as few circuit components common to the primary command electronics as possible. The final command channel assignments for AO-C are listed below.

LIST OF COMMAND FUNCTIONS FOR AO-C

1. 2 mx/10 mx translator on.
2. 2 mx/10 mx translator off.
3. 435 MHz beacon transmitter on.
4. 435 MHz beacon transmitter off.
5. Code store—run mode.
6. Code store—load mode.
7. Morse code telemetry encoder—high bit rate (20 w.p.m.).
8. Morse code telemetry encoder—low bit rate (10 w.p.m.).
9. Translator a.g.c. loop enabled.

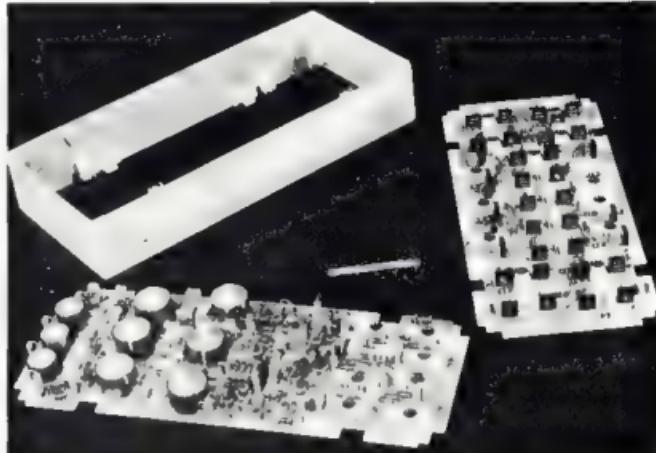


Fig. 4—A photograph of the AO-C Command Decoder. The photograph was taken before all the interboard wiring was installed. The module housing is shown at the back of the photograph.

developing after a period of time. Dry joints can best be eliminated by using the correct solder (a 83% tin 17% lead composition solder with a non corrosive resin core) and a constant temperature soldering iron. To prevent damage of the decoder during the high vibration and acceleration experienced during launch most components are mounted hard down on the circuit boards. As this is not always possible, the decoder will need to be potted in polyurethane foam.

As can be seen in Fig. 4, all the digital integrated circuits carry a unique serial number. This is because they have all been tested by the manufacturer to full military specifications. The rest of the components used in the decoder are all manufactured to military specifications and have been qualified by N.A.S.A. for use in space.

Having designed the command system, we are now in a position to allocate command channel assignments. To

10. Translator a.g.c. loop disabled.
11. Command code store to modulate 435 MHz beacon.
12. Command morse code telemetry encoder to modulate 435 MHz beacon.
13. Command code store to modulate translator beacon.
14. Command morse code telemetry to modulate translator beacon.
15. Disable commands 13 and 14/enable clock sequence (switches between code store and telemetry once every 15 minutes).
16. Enable command 13 or 14 (which ever was last commanded)/disable clock sequence.
17. Reset clock.
18. 2 mx/10 mx translator on (redundant).
19. 2 mx/10 mx translator off (redundant).
20. 435 MHz, beacon transmitter on (redundant).
21. 435 MHz, beacon transmitter off (redundant).

FIG. 3 A COS/MOS INVERTER SCHEMATIC

THE AMSAT OSCAR-C TELEMETRY SYSTEM

G. N. LONG,* VK3YDB
Chairman, Project Australis Group

- The purpose of this article is to explain some of the characteristics of the American 24-channel c.w. telemetry system.

The satellite AO-C will carry the following radio and pulse equipment:

- (a) Two metre to ten metre trans-
lator.
- (b) Australis 21-channel command system.
- (c) The American c.w. 24-channel telemetry system.
- (d) The American code-store system.

This is the first time that this system is being flown on any satellite and its results will be closely examined to see how it compares with the Australis r.t.t.y. telemetry system which is due to fly in the AO-B satellite.

At this stage it should be made clear that the telemetry is purely for house-keeping. It is not intended that the Amateur population should decode the information and send it in. For this satellite this is unnecessary and will cause confusion; i.e. my postman will get very upset!

The telemetry from the satellite will be transmitted in a three-figure code, in which the first number relates to the channel number and is therefore disregarded as far as actual information is concerned.

For example, I will now quote from the Amsat Newsletters for March and June 1972:

SAMPLE TELEMETRY FRAME

(Simulating AO-C Flight Data)

HI	153	132	102	141	
202	235	200	263		
352	380	368	355		
457	452	453	458		
558	524	530	500		
633	600	687	650	HI	

Using the above data one can answer the following questions (remember to drop the most significant digit which is used for data line identification and is not part of the telemetered value):

- What is the approximate spacecraft attitude relative to the sun line? Which faces are being illuminated?
- What is the total power being generated by the solar arrays at the instant the measurement was made?
- Is the spacecraft running on a positive power budget at the time the measurement was made? (i.e. is the battery being charged or discharged?)
- What is the state of charge of the battery? This is a function of the battery voltage (unregulated bus voltage)
- What is the change of temperature (thermal gradient) across the space-craft?

- Is the temperature of the power amplifier transistor running at a temperature very close to that of the spacecraft baseplate? (This will influence the p.a. efficiency.)
- What is the translator usage at the time of the measurement? Is the activity high or low?
- At what efficiency is the translator power amplifier running? (The p.a. runs from the 24v. unregulated bus.)
- What is the status of the 435 MHz beacon?
- Does the telemetry encoder appear to be in calibration?

If you have bothered to work out the telemetry values of the sample telemetry frame, using the calibration data, you should have reached the following conclusions:

Channel (Counts)	Telemetered Value	Parameter	Value
1*	53	I_T	255 mA.
2	32	I_{+X}	32 mA.
3	92	I_{+Y}	4 mA.
4	41	I_{+Z}	164 mA.
5	02	I_{-X}	2 mA.
6	35	I_{-Y}	70 mA.
7	00	I_{-Z}	0 mA.
8	63	I_{SAT}	+130 mA.
9	52	$V_{T_{\text{SAT}}}$	24.2 V.
10	80	V_{SAT}	12.0 V.
11	68	V_{BB}	10.2 V.
12	55	T_{SAT}	15.0°C.
13	57	T_{BB}	12.0°C.
14	52	T_{PA}	19.0°C.
15	53	T_{+X}	17.8°C.
16	58	T_{+Y}	10.5°C.
17	58	T_{+Z}	10.5°C.
18	24	I_{PA}	128 mA.
19	30	$V_{T_{\text{PA}}}$	9.0 V.
20	00	Spare	—
21	33	P_{OUT}	1.09 W.
22	00	P_{OUT}	0.00 W.
23	87	V_{BB}	2.62 V.
24	50	Cal.	50 counts

* Corrected.

Telemetry values associated with the solar arrays and the spacecraft battery should be checked first since they are the most critical values for maintaining the spacecraft. Problems in the power system obviously affect all of the operating systems. The current available from the solar arrays is used either to charge the battery or is delivered to the loads within the spacecraft. Of these loads the translator and the 435 MHz beacon draw most of the current. We can thus write:

$$I_T = I_{\text{SAT}} + I_{\text{TRANSLATOR}} + I_{\text{BEACON}}$$

Using the sample data (current in mA.):

$$265 = 130 + 120 + 0 + I_{\text{BEACON}}$$
$$\therefore I_{\text{BEACON}} = 15 \text{ mA.}$$

This miscellaneous current is used to power the instrumentation switching regulator which provides regulated voltages to all of the sub-systems. The

terms of this equation change continually throughout the orbit. As an example, when Oscar 6 is in eclipse the solar array current will be zero and all of the current must be supplied by the NiCd battery. Since the battery will be discharging during this period the I_{SAT} channel will be negative. The battery voltage from the sample data is 24.2 volts. Since there are 18 separate cells the voltage per cell is 1.32 volts. When fully charged the voltage of a NiCd cell is about 1.38 volts, giving a total battery voltage of about 25 volts. So for this example the battery is a fully charged condition.

The battery voltage should not be allowed to go below 20.0 volts or about 1.1 volts per cell. The battery may also be checked by observing V_{SAT} or one-half of the battery voltage. From this measurement we can tell if each half of the battery is approximately at the same potential. In our example, it appears that two halves of the battery are balanced within 0.2v., which is about the resolution of the telemetry encoder. (Keep in mind that the encoder is digital in nature and the accuracy is ± 1 count.)

Now that we are sure that the total array current is normal, each array should be checked separately for its output. It is noted that the $+X$, $+Z$ and $-Y$ faces all are reading a substantial current, indicating they are the panels being illuminated by the sun. The $-X$, $+Y$ and $-Z$ faces in our simulation are reading slight currents which would be due to the earth's albedo or reflected solar energy.

If we sum the current from each array we obtain: 32 mA. + 4 mA. + 164 mA. + 2 mA. + 70 mA. + 0 mA. = 272 mA., which is slightly higher than the measured value for I_T (Channel 1). Recall that the measurements for each panel were not made simultaneously but were sampled over a period of several seconds. The spacecraft has rotated during this time (a considerable amount just after launch) so that perhaps the current from the $-Y$ panel has increased since the $+X$ and $+Z$ measurements were made. Only after several months in orbit when the spin rate is near zero should these two data compare closely.

This suggests, then, that the orientation of the spacecraft can be determined by knowing the current from the array. Actually this is quite easy to do because we are assisted by a simplifying characteristic of solar cells. The current available from a given panel is proportional to the cosine of the angle between the sun and the normal to the panel. This relationship holds for angles between 0 and 90°. Each panel has a maximum current which occurs at normal incident illumination (0° sun angle) at a given temperature. The

angle of each panel relative to the sun line is then simply:

$$\cos \theta_x + \cos \theta_y + \cos \theta_z = \frac{I \text{ measured}}{I \text{ max}_x + \text{ max}_y + \text{ max}_z}$$

To check the results of these calculations, we may use a characteristic identity of direction cosines:

$$\cos^2 \theta_x + \cos^2 \theta_y + \cos^2 \theta_z = 1$$

This identity, of course, will not hold exactly until the satellite spin rate is very low for the reasons given above. Inaccuracies in these spacecraft attitude estimates will result from changes in the values of I_{max} . The maximum array current changes as a function of temperature and time in space. It should be possible, however, to determine the spacecraft's exact orientation to $\pm 5^\circ$ during the first few months of the AO-C lifetime.

Observing the temperature within the spacecraft will give important information. As with Australis-Oscar 5, the $+X$, $+Y$ and $+Z$ face temperature will be several degrees warmer in the sun than when the panel is looking into space. A periodic temperature function will be noticed by plotting the $+Y$ and $+Z$ temperature data; since this is the spacecraft spin axis. In our simulation the $+X$ face was warmer since it does not experience rotation in and out of the sun on a short term basis. The temperature difference from inside the satellite to its outer surface (the ther-

mal gradient of the structure) is of importance to us. Using the baseplate temperature we can calculate the gradient along each axis.

$$\Delta T_x = T_{+x} - T_{-x} = +5.8^\circ\text{C}$$

$$\Delta T_y = T_{+y} - T_{-y} = -1.5^\circ\text{C}$$

$$\Delta T_z = T_{+z} - T_{-z} = -1.5^\circ\text{C}$$

The temperature of the final translator in the 2 metre/10 metre translator is of considerable importance. For good efficiency this temperature should be nearly equal to the base-plate temperature (about 1 or 2 degrees higher); in our example a difference of 7.6°C is indicated. If this were an actual measurement a problem would be suspected and the translator would probably be turned off by command.

In order of priorities the translator operation is second only to the power system performance parameters. If we check its performance in the simulation we note that the r.f. power output is 1.09 watts. The d.c. input to the final amplifier is calculated by multiplying the unregulated bus voltage (battery voltage) by the emitter current of the power amplifier transistor (Channel 18).

In the example given:

$$I_{\text{PA}} \times V_{\text{BUS}} = 2.90 \text{ Watts}$$

The translator's p.a. efficiency is then:

$$\text{Eff}_{\text{PA}} = \frac{P_{\text{RF}} \text{ (out)}}{P_{\text{DC}} \text{ (in)}}$$

Chan. No.	Parameter	Unit	Parameter Range	Final Calibration Data/Comments*
1A	Total Array			
1B	+X Solar Panel	I (mA.)	0 to 500 mA.	$I_x = 5.00 \text{ N (mA.)}$
1C	-X Solar Panel	I (mA.)	0 to 100 mA.	$I_{-x} = 1.00 \text{ N (mA.)}$
1D	+Y Solar Panel	I (mA.)	0 to 100 mA.	$I_{-y} = 1.00 \text{ N (mA.)}$
		I (mA.)	0 to 200 mA.	$I_{+y} = 2.00 \text{ N (mA.)}$
2A	-Y Solar Panel	I (mA.)	0 to 184 mA.	$I_{-y} = 1.94 \text{ N (mA.)}$
2B	+Z Solar Panel	I (mA.)	0 to 370 mA.	$I_{+z} = 3.72 \text{ N (mA.)}$
2C	-Z Solar Panel	I (mA.)	0 to 370 mA.	$I_{-z} = 3.68 \text{ N (mA.)}$
2D	Bat. Charge or Discharge			
		I (mA.)	-500 to +500 mA.	$I_{\text{BAT}} = 10.00 \text{ N} - 500 \text{ (mA.)}$
3A	Unregulat. Bus	V	12.4 to 30 V.	$V_{\text{BUS}} = 0.174 \text{ N} 12.4 \text{ (Volts)}$
3B	Half Battery	V	0 to 15 V.	$V_{\text{BAT}} = 0.161 \text{ N} \text{ (Volts)}$
3C	Switching Reg.	V	0 to 15 V.	$V_{\text{SW}} = 0.147 \text{ N} \text{ (Volts)}$
3D	Battery Temp.	°C	-30 to +50°C	$T_{\text{BAT}} = -1.471 \text{ N} + 95.79 \text{ (}^\circ\text{C)}$
4A	Base-plate Temp.	°C	-30 to +50°C	$T_{\text{BP}} = -1.471 \text{ N} + 95.79 \text{ (}^\circ\text{C)}$
4B	Translator P.A. Temp.	°C	-30 to +50°C	$T_{\text{PA}} = -1.471 \text{ N} + 95.79 \text{ (}^\circ\text{C)}$
4C	+X Panel Temp.	°C	-30 to +50°C	$T_{+x} = -1.471 \text{ N} + 95.79 \text{ (}^\circ\text{C)}$
4D	+Y Panel Temp.	°C	-30 to +50°C	$T_{+y} = -1.471 \text{ N} + 95.79 \text{ (}^\circ\text{C)}$
5A	+Z Panel Temp.	°C	-30 to +50°C	$T_{+z} = -1.471 \text{ N} + 95.79 \text{ (}^\circ\text{C)}$
5B	Translator P.A. Emitter	I (mA.)	0 to 500 mA.	$I_{\text{EA}} = 5.00 \text{ N (mA.)}$
5C	Transla. Sw. Reg.	V	0 to 30 V.	$V_{\text{SW}} = 0.30 \text{ N (Volts)}$
5D	Instr. Sw. Reg.	I (mA.)	3.8 to 63.8 mA.	$I_{\text{ISA}} = 0.601 \text{ N} + 3.80 \text{ (mA.)}$
6A	Translator R.F. Power	W	0 to 10 W.	$P_{\text{OUT}} = 0.001 \text{ (N)}^2 \text{ (W.)}$
6B	435 MHz. Beacon R.F. Power	mW.	0 to 1 W.	$P_{\text{OUT}} = 0.10 \text{ (N)}^2 \text{ (mW.)}$
6C	Translator A.G.C.	V	0 to 3 V.	$V_{\text{AGC}} = 0.03 \text{ N (Volts)}$
6D	Mid-range Cal.	V	0 to 1 V.	$N = 50 \text{ counts} \pm 1$

AO-C Data to be Telemetered by the Morse Code Telemetry System.

* N = Value Telemetered (omit first digit, which identifies the data line number)

- 1.09
- 2.90
- 37.5%

which is slightly higher than we are presently expecting and disagrees somewhat with what we would expect given the thermal problem mentioned earlier.

The a.g.c. loop voltage is quite high (2.62 volts out of a possible 3.00 volts) indicating the translator is heavily loaded. This can also be near the maximum value. From the beacon power output and the current balance equation it can be seen that the 435 MHz. beacon transmitter is off.

Channel 24 of the telemetry encoder is a calibration channel for the encoder itself. A voltage reference of 0.5 volt is measured on this channel and the encoder should respond with an output of 50 counts (± 1 error count). This 0.5 volt reference is used for all of the thermistors as well and has been very carefully regulated. This channel will allow us to recalibrate the encoder in flight should this become necessary.

PRE-LAUNCH ORBITAL DATA

ITOS-D orbital elements for middle of window (1731z), October 11, 1972,

Epoch 18h26.92 m.
Semi major axis 7839.845 km.
Eccentricity 0.000257.
Inclination 101.780°.
Mean anomaly 265.920°.
Argument of perigee 78.401°.
Motion of arg. of perigee -1.9168° day.
Right asc. of ascending node 297.548°.
Motion of right ascension $+0.9882^\circ$ day.
Anom. period 115.13799 min.
Height of perigee 1459.66 km.
Apogee 1483.70 km.
Velocity at perigee 25876.0 km/hr.
Velocity at apogee 25663.0 km/hr.
Geogr. lat. of perigee -73.539° W.
Local time of ascending node 2106.07.
Local time of descending node 0906.06.
Longitude increment 28.81° /orbit.

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SATELLITE TRACK CALCULATOR

(continued from page 3)

cycle of orbits. Rotate the track so that the start of an orbit is at 173°W and assume the time is 1800 E.A.S.T.

Study the track and see that at 1 hr 42 m. after the start it passes over ZL and to the east of VK to cross the equator at 201.8°W at 1955 hrs. Now rotate the perspex so that the start is now over 201.8°W to see the track for the next orbit. This will now be over VK and the times between a.o.s. and l.o.s. can be seen from where the track crosses the 0° elevation range ring, centred on your location, as well as the intermediate bearings and time.

Try the correct range ring for other locations to see the amount of overlap and whether the satellite will be in this overlap and at what time. Rotate the track around in 2.8° increments to see the other portion of the track that goes N-S. Continue to rotate the track around to find the next day's orbits. These will not be in the same place, but will appear to be further to the west and later by 55 minutes, but a pattern can be derived to make day to day predictions easier.

From Table 1 it will be seen that the tracks will be almost in the same position every second day and 5 minutes earlier. This may not be wholly true in practice as a variation of the nominal period of 0.1 minute will alter the time over two days by 2.5 minutes. The predictions can of course be updated by the time differences found in practice.

Orbit	Time	°W
100	1800	173
101	1955	201.8
113	1855	188.7
114	2050	215.5
125	1755	171.8
126	1950	200.4
139	2045	214.1
140	2245	242.9

Table 1.

USING THE PREDICTION INFORMATION

Generally following a satellite by beam swinging for maximum signal is unsatisfactory, especially for the lone operator who may be attempting to make a QSO at the same time. Due to the relative broadness of a typical 29 MHz. beam compared with the associated 144 MHz. beam, when using AO-C, a good signal could be received when the 144 MHz. beam is off the peak for transmission into the satellite.

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To prepare for a particular pass, from the calculator find the bearing and times at a.o.s. and thence at two or three minute intervals up to l.o.s. Start with the aerial array at the first bearing and step it around at the correct times to the predicted bearings. Continue to do this even if the signals are weak or inaudible. The equipment set-up should ensure that the 29 MHz. output can be monitored while transmitting on 144 MHz. This enables you to listen for your return signal from the satellite and a check can be made of the correctness of the beam heading if desired.

ACKNOWLEDGMENTS

I wish to thank L. Dow, VK7ZLD, for his help in drawing up the calculator and for the encouragement given to me by other local Amateurs when shown the calculator in the embryo state.

REFERENCES

1. "Satellites and Scientific Research," Demand King-Hale.
2. "The Oscillator," "CQ" August 1965.
3. "Oscar Predictions," March 1965.

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A SOLID STATE ELECTRONIC KEYER

I. E. HUSER,* VK5QV

A not-too-difficult approach to the production of an all-electronic automatic key. Seven transistors and sundry other components, plus a few easily provided bits of hardware, result in a device which does all and more than the old electro-mechanical "bug" with no moving parts except the activating paddle.

With the acquisition of an FT200 transceiver, it was felt that a more suitable "shack" than the shed at the end of the garden should be sought. After a little "brainwashing," the XYL (with some reservation) allowed the rig to be installed in a corner of the bedroom—the loungeroom being definitely out of the question.

Headphones were installed so that the "banging, crashing, and good-day Jack I'm using, so and so gear and the weather is lousy, etc." (the XYL's words) would not irritate anyone. So to achieve complete silence when working DX late at night, it was decided

that a completely solid-state key should be obtained.

Having read an article about a simple electronic key using two relays and a handful of parts, a key was built and it worked just as the article said it would. However, it was decided that better results might be obtained if the relays were eliminated, and so the challenge presented itself.

By using basic logic circuits, and burning a little "midnight oil," a solid-state keyer capable of keying the FT200 directly without the use of a relay was built.

CIRCUIT OPERATION

With reference to Figs. 1 and 2, it can be seen that the keyer circuit consists basically of two multivibrators, controlled by gates, and a keying transistor. The free-running multivibrator (Q1-Q2) produces a series of square pulses having a 1:1 mark-space ratio; the repetition rate, and hence the keying speed, being continuously variable between set limits by the 50K variable resistor in the multivibrator timing circuit. The output from this multivibrator is fed to the keying transistor (Q7) to produce a series of

"dots," each having the correct length and the correct spacing between them.

The bistable multivibrator (Q4-Q5) is triggered by pulses derived from the free-running multivibrator, and produces a square-wave output with a 2:1 mark-space ratio which is also fed to the keying transistor. The outputs from both multivibrators are thus combined to produce dashes of correct length and correct spacing (see Fig. 3).

With the paddle in the neutral position, both multivibrators are held off by the gating transistors (Q3-Q4) and no output is obtained from the keyer. If the paddle is moved to the "dot" position, gating transistor Q3 ceases to conduct, the clamp is removed from the free-running multivibrator and a series of dots will be produced for as long as the paddle is held in this position. If the paddle is moved to the "dash" position, the clamps are removed from both multivibrators and their combined outputs produce the required dashes.

It should be noted that gating is so arranged that once a dot or dash has been initiated, it will be completed together with the following space irrespective of the position of the paddle.

* 5 Mugford Street, Mt. Gambier, S.A., 5290.

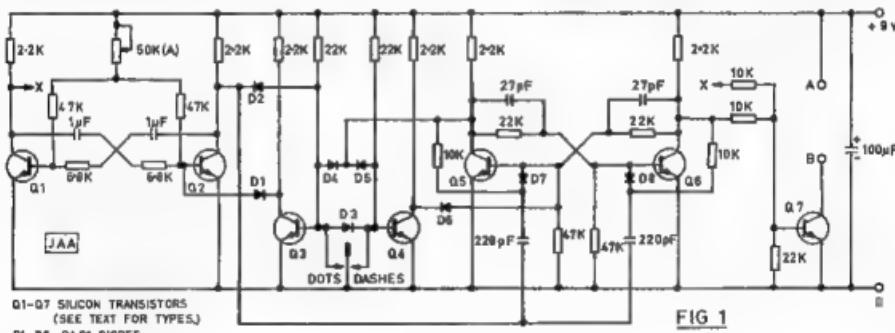


FIG. 1

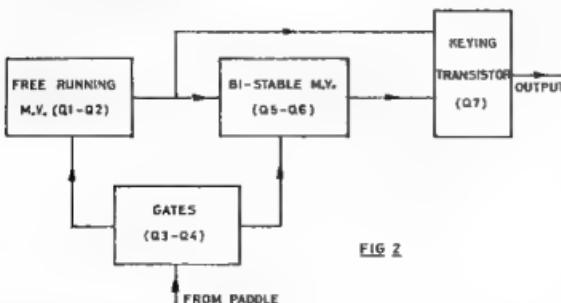


FIG. 2

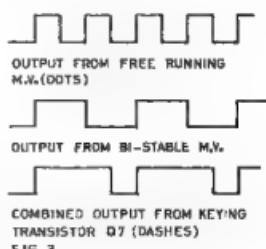


FIG. 3

Hence it is a relatively simple matter to produce "copy book" Morse.

The output from the keyer (terminals A and B) could be used to operate a relay if so desired; however by suitably modifying the circuitry and choosing a suitable keying method, the device can be made to key directly a transmitter or tone oscillator.

CODE PRACTICE

It is desirable that a method of code practice be available to operators new to electronic keyers before they go "on the air".

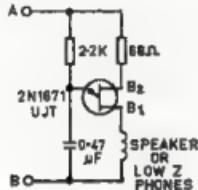


FIG 4a PRACTICE OSCILLATOR

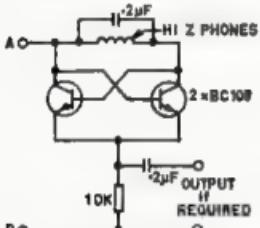


FIG 4b PRACTICE OSCILLATOR

Fig. 4 shows two circuits which can be connected between terminals A and B of the keyer for this purpose. Circuit values may have to be changed slightly to obtain a suitable tone consistent with the amount of inductance in circuit and the likes of the individual operator, etc. Either PNP or NPN transistors can be used in the circuit shown in Fig. 4b, bearing in mind that points A and B will have to be reversed when using PNP transistors to maintain correct polarity to the circuit.

TRANSMITTER KEYING

Fig. 5 shows how the keyer can be used in conjunction with an SCR to

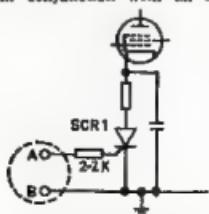


FIG 5 CATHODE KEYING OF LOW POWER STAGE

key the cathode of a low power stage of a transmitter. However, to ensure reliable turnover, it is necessary that the cathode current of the tube be somewhat less than the holding current of the SCR used. Since the holding current for a low power 400 volt SCR is typically in the region of 10 mA, a stage having a low cathode current must be available.

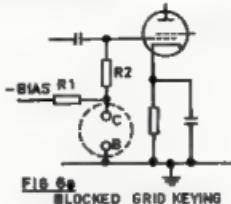


FIG 6a BLOCKED GRID KEYING

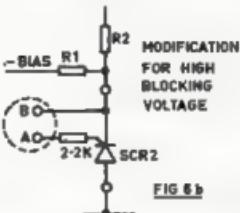


FIG 6b

In Fig. 6a, the keying transistor conducts under "key down" condition to remove blocking bias from the tube. Note that with this circuit the keying transistor must be able to withstand the "key up" voltage and it is suggested that a BC107 might be used for keying voltages up to say 40 volts. If PNP silicon transistors are used in the keyer, then a BC177 could be used as the keying transistor and point "C" would be more conveniently placed at ground potential. (N.B.—The diodes and rail polarities, etc., must be reversed when using PNP transistors.)

For blocking voltages greater than 40 voltages, the circuit in Fig. 6b could be tried if a suitable high voltage transistor is not available.

KEYING THE "FOX TANGO TWO HUNDRED"

When using the keyer in conjunction with an FT200 transceiver a high volt-

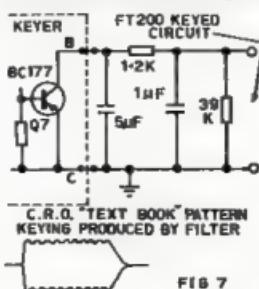
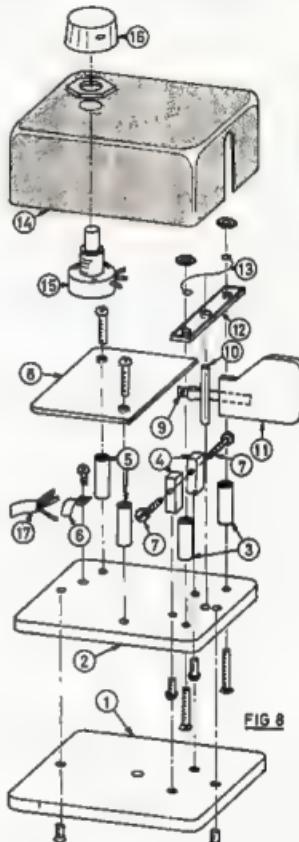


FIG 7

age transistor or the SCR circuit of Fig. 6b should be used since the "key up" voltage is in the region of 100 volts.

However, a small cheap low voltage transistor can be used if a 3.9K resistor is wired across the key socket. This has the effect of reducing the "key up" (continued on page 16)



MATERIALS LIST

Part No.	Description and Material
1	Base plate—1/8" thick mild steel or brass plate
2	Sub-assembly plate—1/8" thick bakelite or perspex.
3	Tubular spacers—brass tubing or bakelite.
4	Contact stems—brass—(obtained from polarised relay)
5	P.C.B. standoffs—bakelite.
6	Cable clamps—brass, aluminium, etc.
7	Contact screws—obtained from polarised relay
8	P.C.B.—P.C.B. or Veroboard
9	Double-acted contact—obtained from polarised relay
10	Paddie pivot—1/8" silver steel
11	Paddie's hand—3/16" bakelite or perspex.
12	Control knob—3/4" bakelite or perspex.
13	Connecting cable—shielded multi-core cable.
14	Cover—suitable plastic box
15	Speed control—60KA potentiometer.
16	Control knob—any suitable knob
17	Connecting cable—shielded multi-core cable.

AN INTEGRATED CIRCUIT I.F. STRIP

JOHN E. DUNKLEY,* VK5JE
(Ex VK5ZJD)

- An outboard i.f./detector strip suitable for improving the selectivity of a receiver for r.t.t.y. reception.

Having recently become interested in the r.t.t.y. mode of communication, it did not take me long to realise that my communications receiver needed some additions and/or modifications or it "had to go". After extensive modifications to the power supply (adding VR tube), b.f.o. and taking care of some mechanical details, the drift problem was made bearable but the set itself lacked the ability to be selective enough for close channel reception of r.t.t.y. transmissions. In conditions of crowded Amateur bands, perfect copy of r.t.t.y. transmissions was almost impossible.

The 120 pF capacitors across the input and output coils of the mechanical filter should be 5% types or better and preferably high stability types, e.g. silver mica (SM). The IC is conventionally wired and do not forget the capacitor (0.1 μ F) from pin 2 to earth. An R.C.S. type 178 455 kHz i.f. transformer was used to couple the output of the IC to the product detector. This unit was used because it was in the junk box but other types could be used without circuit modification. This particular type is one of the larger variety i.f. transformers as used in the miniature valve mantle sets, but if size is a problem a miniature "transistorised" version could be substituted.

The product detector is one which works very well with a minimum number of parts and provided the b.f.o.

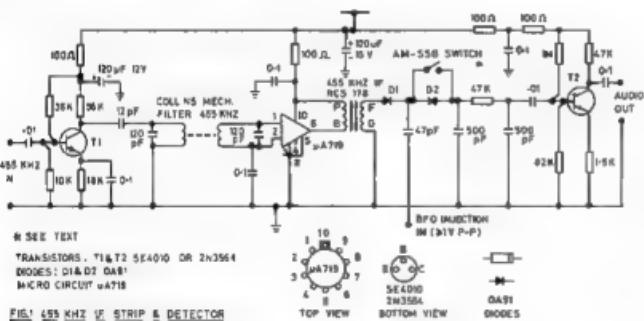


FIG 1 455 kHz I.F. STRIP & DETECTOR
TRANSISTORS: T1-T2 2SA4010 OR 2N3564
DIODES: D1-D3 1N5818
MICRO CIRCUIT uA719

It was decided that an outboard i.f. strip and detector would be a good start to "updating" the receiver side of the shack equipment, and would also be a good interim start for an all transistorised a.f.c. controlled receiver for serious r.t.t.y., c.w., s.s.b. copy. Having decided that the i.f. strip would be a good place to start this project, things started to move.

The heart of the i.f. strip is a 455 kHz mechanical filter having a pass band of 2.1 kHz. This is followed by a Fairchild IC type uA719

Looking at the circuit (Fig. 1) we find that the first active device, T1, provides some amplification at 455 kHz and also provides the correct matching for the mechanical filter. It should be pointed out that the coupling to the mechanical filter is done by a 12 pF capacitor and this value is the **maximum** that can be used if the pass band characteristic of the filter is to remain unchanged.

to anything, however a 50K ohm potentiometer connected between pin 4 of the IC to earth provides a manual i.f. gain control (see Fig. 2). A 0.01 μ F capacitor connected from pin 4 to earth (provision for mounting this is provided on the p.c. card) takes care of any possible instability problems. This capacitor need not be used if the manual gain control is not incorporated.

A second independent amplifier providing some 30 dB of gain is also available in this IC and although not used in this i.f. it is "earmarked" for use in the a.f.c. unit mentioned at the beginning of this article.

The leads to the a.m.-s.s.b. switch should be kept as short as possible, preferably shielded and the switch is normally open for s.s.b. and c.w., and normally closed for a.m.

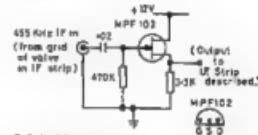


FIG 3 FET DRIVER

The alignment procedure is about as simple as anyone could ask for. It involves providing a 455 kHz modulated signal at the centre of the mechanical filter passband, selecting the a.m. switch position and monitoring the collector of T2 with a c.r.o. or a.c. voltmeter and adjusting the primary and secondary slugs in the i.f. coil for maximum reading. Measuring the d.c. current drawn (20 mA) will give a good indication that all is well. The input signal to the i.f. for this alignment need only be in the region of 10 μ V. When aligned, a 1 μ V 455 kHz signal is detectable.

To connect the i.f. strip to a valve type receiver a FET driver can be added to the receiver. A suitable driver is shown in Fig. 3. Note: The driver unit should be mounted within the valve receiver.

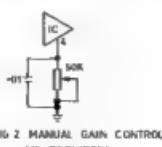


FIG 2 MANUAL GAIN CONTROL
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A SOLID STATE ELECTRONIC KEYER

(continued from page 14)

voltage to approximately 30 volts without affecting the keying characteristics of the transmitter, thus allowing transistors such as the BC107 (NPN) and the BC177 (PNP) to be used.

The FT200 is renowned for keying transients and this, coupled with the inherent fast switching times of the keyer, caused some problems with "thumping".

Many ideas were tried, and eventually the "brute force" filter shown in Fig. 7 was adopted and wired in place of the original Yaesu filter. Values appear to be fairly critical, but a keying characteristic with a slight "thump" on the make and a clean break was obtained using the values shown.

CONSTRUCTION

The keyer can be built using the hand tools normally found in the experimenter's workshop. Fig. 8, together with the materials list, should give intending "smoke signallers" a good idea of construction, however a few points should be made:—

1. The size of the keyer is necessarily a function of the box available and since the original was built around a plastic box of dubious origin, measurements have purposefully been omitted.

2. The fixed and moving contacts were obtained from an old P.M.G. polarised relay which had been lying in the junk box for many years. A few of these are still available through disposal houses at a reasonable price.

3. All the electronic components were mounted on "vero-board" which fitted neatly inside the keyer. A printed circuit board of course would make for a neater job.

4. If steel or brass is used for the base plate, a piece of 1/32" sheet rubber glued (with contact adhesive) to the underside will prevent any tendency to slip even on quite smooth surfaces.

FINAL COMMENT

The arrangement used at VK5QV is the tone oscillator shown in Fig. 4b (using AC128 transistors) and the PNP keyer. A switch is used to allow the practice and transmitter keying functions to be readily selected. Output from the tone oscillator is fed to a tape recorder so that any practice sessions can be recorded and evaluated.

The unit is powered from 9 volts obtained from a simple transistor series regulator.

Good luck and good DX! •

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NEWCOMER'S NOTEBOOK

With Rodney Champness, VK3UG

The contribution this month is rather short as I am in the process of shifting my home due to the nature of my employment. My thanks to those who have taken the trouble to write to me, with ideas, circuits and requests for help. I may not be in the position to reply to all directly, but I do expect to help via "Newcomer's Notebook" wherever this is possible.

I have an offer from Miles Turner, 45 Kent Street, Kallangur, Brisbane, 4508, of information on the old A.W.A. 709C series of eight-valve seven-wave band receivers. These sets, although bulky and using octal-based valves, should prove to be well worth overhauling. They tune narrow bands, with continuous coverage, from 530 kHz through to 23 MHz. They have an r.f. stage, and in general are built very solidly. The r.f. section is rather cluttered but with care and the use of a small soldering iron, routine maintenance and modification should not cause much trouble.

The addition of a small oscillator bandsplitting capacitor, as mentioned in September "A.R.", and the fitting of a product detector, which will be part of a future issue, would make these rather oldish but well designed sets suitable for the common used h.f. transmission modes.

I suggest you write to Miles if you require data on these sets.

I have been asked by a reader if I could build a converter to go on the front of an old dual-wave receiver. It would certainly be possible, but there are two reasons why I cannot oblige: (1) that my time is restricted, and (2) that it is the aim of "Newcomer's Notebook" to help you to build or assemble for yourself some or all of your receiving or transmitting/receiving station, "One-off" for projects some time in the future may be a possibility.

Some future articles will be on television interference as caused by 6 metre Amateurs, basic test equipment, and learning Morse code. •

* 44 Rathmullan Road, Boronia, Vic., 3155.

CORRECTIONS TO VK-ZL 1972 CONTEST RESULTS

Phone	Section	
VK4AD	14 MHz.	Total
VK4ABC	7000	7000
VK4ED	8270	5370
	3480	3480

AROUND THE TRADE

R. H. Cunningham Pty. Ltd. announces their appointment as exclusive distributors in Australia for the complete line of communications span-ty, star strap, cable ties, harness accessories and allied items manufactured by Paulin Corporation of the U.S.A. Both open and bond stocks are available.

Commercial Kinks

With Ron Fisher, VK3OM

Since starting this column several months ago, the Trio 9R 59DE's receiver has without doubt stirred up the most interest. My incoming mail seems to indicate that there is at least ten times the demand for information on this receiver than there is even for the FT200. Perhaps there is a moral in this, but I must leave our readers to work it out. Therefore this month I am going to publish a few extracts from letters I have received over the last few months. I hope this will enable Trio owners to compare their problems and experiences. However, before getting onto them I intend to continue with the Carphone conversions from Peter Campbell, VK2AXJ.

CONVERSION OF A.W.A. F.M. CARPHONES, Part 2

High-band Carphone to 148 MHz.—Transmitter: Add 8.8 pF. across each winding of TR8. Add 1.8 pF. across L9. Rewind L11 with 4 turns of 16 s.w.g. Remove C94, C115 and relay RL2. Receiver: Add 1.8 pF. to L4.

Low-band MR10B to 52 MHz.—Transmitter: Add 15 pF. across both windings of LT4. Rewind both LT5a and LT5b with 8 turns of 16 s.w.g. Rewind both LT6a and LT6b with 5 turns of 16 s.w.g. Receiver conversion: Rewind L11 with 18 turns of 24 B. & S. and tap at 3 turns from the cold end. Rewind T1 in the same way. Add capacity across T9 until it resonates at 40 MHz.

Low-band MR10C and MR26A to 52 MHz.—Transmitter conversion: Add 15 pF. across both windings of T11. Rewind L11 with 8 turns of 16 s.w.g. 5/16" diameter and 4" long. Rewind L12 in the same way. Rewind L13 with 6 turns of 16 s.w.g. 9/16" diameter and 4" long. Increase C125 to 100 pF. Receiver: Add 4.7 pF. to L1, 3.3 pF. to L2 and L3, and 10 pF. to L4 and L5.

Low-band MR20B to 52 MHz.—Transmitter conversion: Add 15 pF. to both L8 and L9. Rewind L11 with 5 turns, L12 with 18 turns and L15 with 10 turns. Receiver: Add 4.7 pF. to both L1 and L2. 3.3 pF. to L3, 10 pF. to L5 and L6. Increase C8 to 39 pF., but note that this value is critical and may vary on some units to achieve neutralisation.

In all the preceding modifications coils should be wound with the same diameter and spacing as the original unless otherwise specified.

If the narrow band filter, type 5Q57975, is removed and replaced with the wide band filter, type 3Q57975, the 2.2 pF. condenser across the input and output of the filter should be removed.

That completes the carphone data for the time being, but don't forget that circuits will continue to be available in the usual way.

THE TRIO 9R 59DE/DS

My thanks to all who have written to me with your ideas and comments about

* 3 Fairview Avenue, Glen Waverley, Vic. 3150.

these receivers. Without exception, owners are generally happy with the performance of their sets. However, the Trio is very adaptable to small modifications similar to those covered in past issues of "Amateur Radio". One such change is a better tube in the r.f. stage in place of the 6BA6. There are several possibilities, the first being the 6BZ6. This would give a worthwhile lift in gain and only one small circuit change is necessary. Remove the earth connection to pin two of the r.f. tube V1. Now connect pin two to pin seven with a short piece of insulated wire. It is now possible to plug in either the original 6BA6 or the new 6BZ6.

A better choice, however, would be the EF183/SEH7. This tube has a transconductance of 12,500, nearly three times that of the 6BA6. To instal this tube in the Trio it is necessary to remove the existing 7-pin socket and replace it with a 9-pin socket. With such a hot tube some additional shielding is needed. Cut a piece of light gauge tin plate about 1" high and 1½" wide. Position this across the socket and solder it to pins 5, 6, the centre earth spigot and the nearby earth lug. The tube can now be wired up to the original circuit.

Chas Otheren, VK5ON, reports some of his experiences. After making all the power supply improvements so far described, an extra electrolytic across the first section of C42 reduced the hum a further 50%. Chas used 16 µF., but I would think that 50 µF. would not be out of the way.

The b.f.o. developed trouble after about 12 months' use. It would either drift off frequency or drop out of oscillation altogether. After much searching, Chas traced the trouble to a 1,000 pF. 125v. condenser across the b.f.o. coil. This was replaced with a 1,000 pF. 600v. styrofoam type.

He also reports improved reception with the help of a VK5AX preselector. This unit enjoyed great popularity during the mid 1950s, and was unique in that it tuned from 3 to 30 MHz. without the need for band switching. Apart

from the extra gain, the front-end selectivity would be increased with a reduction in images on the higher bands.

An interesting modification comes from A. Graham, VK6ZCQ. He has transposed the b.f.o. and the i.f. input connections to the product detector V6 and says that this gives a more constant b.f.o. level. In a letter just received from Alex, he gives details of a cathode follower using the vacant half of the 6AQ8, and I will include circuit details in next month's issue. He reports an improvement in stability with this modification.

Neville Symons, L30448, also reported b.f.o. trouble. In the early 59DEs, the b.f.o. tuning condenser was apparently of poor design. After some use it developed wear and consequent frequency instability. Neville replaced this with the later type, which is the same as the one used for the antenna trimmer. Neville also improved warm-up drift by moving the OA2 regulator to the socket position intended for the calibrator tube. If you have already installed a calibrator, some form of heat shield might be worth a try.

I did intend to include some more FT200 modifications this month, but it looks as if I have run out of space again. Next month then, back to the FT200 and even more on the Trio 9R 59DE/DS.



AFTER THOUGHTS

Some after thoughts on F.M. Repeater by Ian Champion, VK5ZIP (see April and May 1972 "A.R.").

1. The power supply was labelled as 0.5 amp.—should be 5.0 amp.

2. Power supply, Pin 8 of the LM330 and the 1 µF. 35v. tantalum capacitor should be shown connected to the collector of 2N3442.

3. Ident control circuit. The collector/base feedback resistors of the bistable pair TR4/TR5 should be 47K ohms not 4K7 ohms. Likewise the tx control circuit.

4. The repeater now identifies as "VK5W1/R1"—25 w.p.m. m.c.w. from a new fully solid state IC keyer (installed January).

5. Sporadic interference from industrial r.f. generating equipment was causing ident ad nauseam. A modification was incorporated such that a minimum of three seconds of input signal was required before the ident circuit recognised its presence.

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Model 2B4-RK3

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Operating radius: about 10 inches

Total height: 23 lbs

Mesh (not included) to 1½" inch o.d.

Element min boom material: heavy wall

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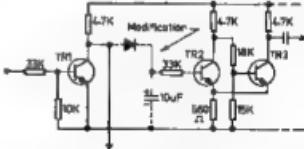
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AWARDS COLUMN

With Geoff Wilson,* VK3AMK

W.I.A.—TASMANIAN DIVISION

V.E.T. GOLDEN JUBILEE AWARD

(1) Radio Amateurs outside Australia and New Zealand to contact five (5) Tasmanian stations (VK7) during the period 1st January, 1972, to 31st December, 1972.

(2) Any licensed Amateur band may be used.

(3) Any Amateur mode of transmission may be used with cross mode being acceptable. Cross band working is not acceptable.

(4) Log entries of the date, calling, time, band and other relevant details signed by the operator and two (2) other licensed Amateurs or by the operator and the Secretary of his Club to suffice for recognition of contacts. Isolated operators who are unable to comply with the above may request their logs be subject to check by the organisers.

(5) A suitable certificate inscribed with the number of Tasmanian stations worked will be issued to the operator as confirmation of the contacts.

(6) To ensure receipt of the certificate, I.R.C.s will be sent with the log as follows: See Mail 3 I.R.C.s, Air Mail 6 I.R.C.s.

(7) Australian and New Zealand stations will be counted as contacts (20) Tasmanian stations with the remainder of the Rules applying except that the QSL Bureaux be used for despatch of certificates unless the operator wanted service in (6) above, when 1 and 2 I.R.C.s respectively will apply.

(8) Address for application of logs: V.E.T. Golden Jubilee Award, Box 8813, G.P.O., Hobart, Tasmania, 7001.

HUNTER BRANCH AWARDS

This certificate, awarded for outstanding performance in radio listening and two-way communications, is now available.

(1) **For QSL Cards.**—Must have been completed during any twelve-month period after 1st January, 1970. Certificates will be awarded in five classes.

(a) **For Overseas Stations.**—Must confirm that five different Hunter Valley Amateur stations have been contacted. No band limitations. Claims to be accompanied by a copy of the log and a declaration that QSL cards to confirm the contacts have been sent.

(b) **For QSL Cards.**—Must confirm that ten different Hunter Valley Amateur stations have been contacted. No band limitations. Does not apply to Amateurs resident in VK1 or VK3 call areas. Claims to be made as in class (a).

(c) **For N.S.W. and A.C.T. Stations.**—Must confirm that twenty different Hunter Valley Amateur stations have been contacted. No band limitations. Claims to be made as in class (a). Except for Hunter Valley stations, must include confirmation in the form of QSL cards.

(d) **For Hunter Valley Stations.**—Must confirm that one hundred different overseas countries have been contacted. No band limitations. Applied only to Hunter Valley stations and is an addition to class (a). Claims must be accompanied by QSL cards.

(e) **For Hunter Valley Listening Stations.**—Must confirm that twenty-four different overseas countries have been legally within the VK1 and VK3 call areas. No band limitations. Log entries must include four stations each of the six continental areas as set out in the International Amateur Radio Union classification. Claims must be accompanied by QSL cards.

How to Claim the Hunter Branch Award.—The Hunter Branch Award may be claimed by submitting the necessary extract and QSL cards if required to:

Hunter Branch, W.I.A. Award Committee, Box 134, P.O., Charltonville, N.S.W. 2290, Australia.

Cost of the Hunter Branch Award Certificate to those applying for it will be \$1.00 if posted M airmail 50 cents if surface mail. The cents M it is collected at Hunter Branch meetings.

Stations defined as being Hunter Valley stations must be established permanently as far as the definition accepted by the Radio Branch of the Postmaster-General's Department within the borders of the Hunter Valley as defined by the Hunter Valley Research Foundation.

The decision of the Hunter Branch W.I.A. Executive Committee will be final.

* 7 Norman Avenue, Frankston, Vic. 3199.

P.M.G. EXAMINATION PAPERS, AUGUST 1972

The following are the questions asked at the last examinations:

SECTION K (REGULATIONS)

(Time allowed—30 minutes)

NOTE. Three questions only to be attempted. Credit will not be given for more than three answers. All questions carry equal marks.

1. (a) State the regulatory requirements regarding the quality of transmissions from an amateur station.

(b) Discuss the responsibilities of the licensee of an amateur station regarding the erection of an aerial mast.

2. (a) Give an example of a distress call sent by:

(i) radiotelegraphy, and

(ii) radiotelephony.

(b) As an amateur station licensee what action would you take upon hearing a distress call?

3. What action should be taken by an amateur station licensee when informed that transmissions from his station are causing interference to the reception of television or broadcast programmes?

4. State the meaning of each of the following "Q" code signals:

QRX QRTT QSY QRU QRH?

TELEGRAPHY

Section L (Receiving)

(Speed—10 words per minute)

Four months ago Venus 8 departed this earth bound for

the searing planet. The 472 degree Celsius heat prevents soft landings by manned craft however a capsule dropped from the spacecraft survived 56 minutes of this heat together with the atmospheric pressure some 50 times greater than

Section L (Sending)

Time allowed—2½ minutes

(Speed—10 words per minute)

This was the second capsule to transmit from Venus. The first lasted 23 minutes and came from the spacecraft Venus 7 in 1970. No man made craft has

SECTION M (THEORY)

(Time allowed—2½ hours)

NOTE.—Be very generous only to be attempted. Credit will not be given for more than seven answers. All questions carry equal marks.

1. (a) Draw the circuit diagram of an amateur station transmitter suitable for operation in the 14 MHz band. Explain briefly the theory of operation of each stage of the transmitter.

(b) Describe how you would tune the transmitter described in (a).

2. Assisted by a circuit diagram, explain the operation of a cascode radio-frequency amplifier suitable for use in a v.h.f. receiver.

3. (a) Describe, with the aid of a sketch, the operation of a type of microphone suitable for use at an amateur station.

(b) Draw a circuit diagram of a solid-state type pre-amplifier suitable for use with a high impedance type microphone.

4. Discuss the limitations of a heterodyne type frequency meter when used alone for measuring frequencies in amateur bands 144 MHz and above. What additional apparatus would you need to measure the frequency does in fact lie in the desired band? Briefly discuss the theory of operation of this additional piece of apparatus.

5. (a) What is a parasitic oscillation and how is it produced?

(b) Why are parasitics undesirable in a transmitter?

(c) Explain the methods you would adopt to locate and suppress them.

6. (a) Explain the possible causes of interference to television receivers from amateur station transmitters.

(b) Discuss the technical precautions you would adopt to avoid interference from a transmitter to television and broadcast receivers.

7. (a) Discuss the factors which affect the D.C. resistance of a conductor.

(b) Explain why the radio-frequency resistance of a conductor may differ from its D.C. resistance.

(c) Describe a method of winding which will minimise inductive effects in a wire wound resistor.

8. (a) Discuss the features you consider an antenna, operating in the 14 MHz amateur band, should possess to enable it to communicate effectively over very long distances.

(b) With the aid of a sketch describe briefly an antenna possessing the features you have outlined in (a).

9. (a) Find the total capacity when three capacitors of 3, 4 and 8 microfarads respectively are connected:

(i) in parallel, and

(ii) in series.

(b) Calculate the capacitive reactance of the series combination in (a) when connected across a 50 Hertz supply.

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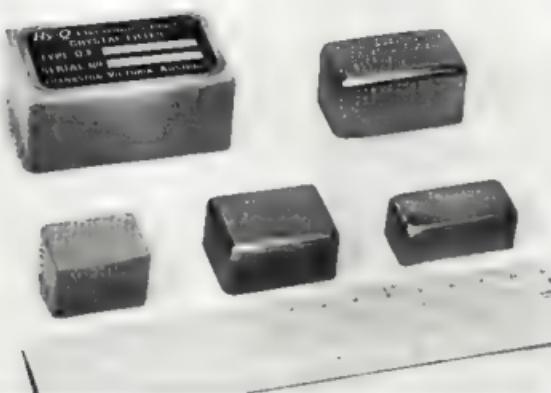
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R.D. CONTEST RESULTS

(continued from page 18)

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TAS.: Video and Sound Service Co. Hobart. Phone 34-1180.
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WESTERN AUSTRALIA

VKA—Phone

ID	556	1280	AW1*	120	260	DZ	35	81
WV	497	1148	TC	68	207	KY	37	77
DX	215	451	WT/P*	75	125	SH	31	67
NE	286	674	ME	55	125	SR	36	76
RS	134	508	KJ	52	118	HT	17	43
PI	303	487	VN	60	125	XC	17	37
MF	175	367	EG	37	87	LF	9	17
			AM	46	87			

VKA—CW

VKA—Open

BC	163	756	CT	809	891
WT	143	848	LG	181	403
RL	43	202	CR	17	62
GA	30	142	HU	10	28
ND	35	92	SM	10	34

VKA—Receiving

B. Dolphin 1873 T. McGrath, L60131 807

TASMANIA

VKT—Phone

JV	568	1287	ZQJ	119	116	DK	10	41
UX/P	255	481	ZIE	113	113	LD	37	57
MS	215	451	ZSF	98	85	NZ	33	55
MZ	125	417	CL	34	84	ZLH	35	55
MX	180	347	AR	30	85	ZCT	33	55
NU/P	215	481	AL	29	85	ZLJ	35	55
AK	117	311	ZWZ	79	79	HT	21	39
KK	155	384	CX	21	86	ZSF	27	57
BM/P	131	364	PS	64	64	FD	25	57
GW	115	300	RP	23	85	ZK	34	54
LE	125	355	PS	50	50	ZEF	15	38
PF	103	144	ZJG	51	50	AZ	10	21
ZIF	143	143	ZPR	44	44	RO	11	21
ZNR	143	143	MK	44	44	ZBE	10	19
VK	63	130	ZEC	43	43	BB	6	8

VKT—CW

CH	163	876	RY	126	408	BJ	31	112
LJ	127	528	CIC	78	236	RD	40	97
GW	128	528	OM	71	236	JB	36	97
MZ	128	417				YL	10	33

VKT—Open

KJ	614	1261	AL	93	94	LW	32	60
BB	222	558	EJ	106	174	QE	26	118
RM	222	558	JA	43	183	ZSY	46	80
BC	81	122				CF	30	45

VKT—Receiving

R. J. Severini 796

NORTHERN TERRITORY

VKA—Phone

VKA—CW

CM	236	775	HA	181	474
CM	206	560	EE	106	424
DI	152	277			
AZ	125	112			
JB	74	112			
KP	18	47			

PAPUA-NEW GUINEA

VKE—Phone

VKE—CW

JK	265	225	VO	82	116
KA	235	565			
DM	265	520			
EV	174	480	VKE—Open		
			DH	303	861

CHRISTMAS ISLAND

VKE

VW—Open

XX	100	344
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ANTARCTICA

VKE

JV—Open

Phone		CW
ZLAIAMIN	470	1066
ZLIAOQ	181	319
ZLIAOQ	181	189
ZM2IACP	181	581
ZM2IACJ	250	480
ZM2IJK	27	
ZM2IABC	263	537
ZM2IABC	217	547

NEW ZEALAND

CW

ZL1DV	58	284
ZL1EQ	94	284

We regret the non-arrival of the results this month caused by the Contributing Editor's change in QTH. Meanwhile a note from K1H6ZFP about the Kure and Midway Islands DX-pedition indicates that W7WDX (K1H6ZFP) and the group will head out of Honolulu about 22nd October and return about 28th October, during and after the "CQ" W.W. DX Test «a.s.b.» on 28th-29th Oct. from Midway. Frequencies given include 14350/14288 kHz, 21280/21300 kHz, and 7205/7200 kHz QSL to K1H6ZFP with three ICRs plus SAE.

Congratulations to David Rankin, VK3QV, upon acquiring the call VK3VIRL.

VHF UHF

an expanding world

With Eric Jamieson, VK5LSP

Closing date for copy: 30th of month.
Times: E.A.S.T.

AMATEUR BAND BEACONS

VK5	53.100	VK6ZVS, Macquarie Island.
	53.100	VK5MA, Mawson.
	53.200	VK6KGR, Casey.
VK3	53.450	VK3SWL, Dural.
VK3	144.700	VK3WL/86, Vermont.
	144.700	VK3WL/100, Tumut.
VK4	144.400	VK4W/1, Townsville.
VK5	144.390	VK4W/1/R1, Townsville.
	53.000	VK5VY, Mt. Lofty.
VK5	144.800	VK5VY, Mt. Lofty.
	53.000	VK5VY, Mt. Lofty.
VK5	144.900	VK5VY, Mt. Lofty.
	53.000	VK5VY, Mt. Barker.
	144.500	VK5VY, Albany.
VK7	144.700	VK5VY, Albany.
	144.700	VK5VY, Albany.
ZL1	145.100	ZL1VHF, Auckland.
ZL2	145.300	ZL2VHF, Wellington.
	145.300	ZL2VHF, Palmerston North.
ZL3	145.300	ZL2VHF, Palmerston North.
	145.300	ZL2VHF, Palmerston North.
ZL3	145.300	ZL2VHF, Palmerston North.
ZL4	145.400	ZL2VHF, Palmerston North.
JA	58.500	JAIIGY, Japan.
	50.100	HL2WU, South Korea.

1 VK6ZVS is again operating from Macquarie Island running 30 watts c.w. to a 3 element beam on Australia. The keying cycle includes a pause when stations may call in.

The listing of VK1VY in Canberra has been removed for the time being. Apparently I was misinformed that it was likely to be *co*-located with the suburban listing. This has caused some problems between the Canberra Radio Society and the P.M.G. Dept. I regret any inconvenience such listing may have caused. In future I shall certainly be more careful in defining the boundaries of the proper operation of any new beacons which may appear before adding to list, that's for sure!

2800 MHz CONTACT—RECORD CLAIMED

Following an 18-month programme of building, testing and modification, a two-way contact was made on Sunday, 3rd December, 1972, between Dick VK2BDN, operating portable at Glenbrook in the Lower Blue Mountains, and Bill VK2ZAC at his home QTH at Narreer, a distance of 25.8 statute miles. The contact commenced at 13.15 p.m. and was broken contact on 1st f.t.s. to allow for up-sets. The signal was maintained for 46 minutes, being limited by Dick's available battery power. Weather conditions were warm and calm, 20 degrees C. with some haze and the optical path lengthened some 1000 m. Signals received were VK2BDN reported 5 x 7 and VK2ZAC reporting 8 x 4. It is understood the previous best Australian Amateur contact on this frequency was 8 miles.

Equipment—VK2BDN: transmitter, 144 MHz exciter plus a series of varactor doublers to 2800 MHz, estimated power output 0.75 watt, 100% efficiency. VK2ZAC: 144 MHz to 2800 co-ax, to a 4-dish dish with dipole feed, crystal controlled converter with 50 MHz 1N5371 mixer, 144 MHz first f.t.s. to a mobile communications receiver.

At VK2ZAC: Transmitter, 144 MHz exciter, 3CK100A2 doublers to 2800 MHz, 3CK100A2 power amplifier 1.5 watts Modulation a.m. Feed-line—due to the need for home station operation at VK2ZAC—the antenna is supported on a lattice tower by means of an elevating truck which may be withdrawn to allow for down-tilting. To reduce feed-line losses a 15-ft. waveguide section plus co-axial transitions was built using 4 x 3 inch galvanised downspine. Antenna 4-ft. dish with dipole feed. Receiver, crystal controlled converter with 50 MHz 1N5371 mixer, first f.t.s. pre-amp to 6 m. 6 m. converter and BC343 h.f. receiver fitted with a gated beam f.m. discriminator.

Congratulations to Dick and Bill for their efforts, and we hope to hear more from them as the operating distances are increased, and thanks to Bill for sending me the information.

—Forreston, S.A., 5333.

BLURB

I'm not trying to be rude! That's the title of the latest news bulletin to reach my office desk, this time from the "V.H.F. and U.H.F. Group" in Mt. Gambier, S.A., under the editorship of Dale VK5DA. Running to 18 pages, it has lots of information, even to including a recipe for a chocolate cake! I hope I may be able to select suitable paragraphs from its pages from time to time which will be of general interest. Good luck S.E.R.G. with the project.

QRM

This is another bulletin, and published by the Northern Zones of W.I.A. in Launceston, Tas., which I am grateful to receive. I note an interesting comment in the last issue regarding the Remembrance Day Contest, and I quote: "In the 1971 V.H.F. Contest, added to the two hourly limit for working a v.h.f. station in the R.D. Contest must be the brain wave of the century. The enthusiasm of Z calls had to be heard to be believed—many of them must have 150 contacts. At approximately 25 different call signs were heard through the Mt. Barrow repeater. Quite a few crystals around for a 'temporary' frequency? Yes, I do believe the Federal Contest Committee has taken a step in the right direction and given v.h.f. operators extra incentive to join in our national contest, and hope they will support the idea."

50 MHz MOONBOUNCE

A letter has arrived at my desk in a very roundabout way through ZL2WVB and VK5AKN asking if I am interested in moonbounce operation on 50 MHz. With Joe Musciano, WASHNK, 6014 South Park Street, Houston, Texas. Actually, while the thought of moonbounce is a good one, it does not seem to be the kind of time required for such a venture and my prevailing noise level is so high as to make very low level signals impossible to read. If there are any others who would like to try with me, I suggest you contact him personally by letter. He runs 50 watts output, and has received his own signals back from the moon.

PORTABLE OPERATIONS

This is the time of the year when operators begin to think about selecting a place for portable operations during the Christmas and New Year break. If anyone has definite details of such operation available by 30th October perhaps you might send the details to me for inclusion in these notes. For December, I am thinking of the Geelong Amateur Radio Television Club bulletin that Mike VK5ASQ is a likely starter around the New Year period. Are there any others?

VHF ANTENNA DAY MEASUREMENTS

The Victorian "VHF-er" for Sept. contains details of 55, 144 and 432 MHz antenna measurements, and serves to indicate the wide range of results which can be obtained by different constructors. Looking over the results the 11 element yagi on an 8-m. f.t.s. boom seems to have good gain for a beam antenna. A figure for this was submitted by VK5AUA. A comment at the end of the results indicated some multi-path problems existed with the tests and caution should be exercised in examining the results. I would suggest that if you have a gain figure for your beam antenna, then have a look at the tabulated results quite worth while, if only further to add to your confusion.

Because you build an Orr and Johnson 16 element for 144 MHz, you might be lucky to get an 8-m. f.t.s. gain or it might be 5 dB. For these results have shown. The golden rule seems to be "follow the specifications rigidly, vary them at your peril if you are not familiar with antenna behaviour".

TWO METRE SSB CALLING FREQUENCY

Also from the "VHF-er" is noted a motion passed at the August meeting of the VK3 V.H.F. Group that a frequency of 144.150 MHz be used as a s.s.b. calling frequency. The idea of a calling frequency is good, but perhaps a final suitable frequency for all Australia might be considered by the present Band Planning Committee.

VHF FIELD DAYS

VK3 will be holding a special Field Day on 31st November, involving a mobile portable multi-site. On 3rd December there will be Field Days in VK3, VK3 and ZL, so perhaps it will be a Field Day for some. The National Field Day is scheduled for 10th and 11th February, 1973. It is time now to start planning for the National Field Day if you are likely to make a big effort and cover all bands.

MOBILE OPERATION

With the holiday season not so far away, many will be giving thought to interstate mobile operation. Bear in mind that for many

years no special permission was needed, but now v.h.f. operation is well as h.f. requires a license from P.M.G. Details of procedure, dates of operation, and other relevant details as required by the Regulations as printed in the Handbook. Play safe, write early. Issue page 2 of this issue. Ed.

That's all the news for this month, and as space in these columns is still subject to pressure from the Editor of "A.R.", no padding is used just to fill space. I close with the thought for the month. "The tough part of politics is to satisfy the voter without telling him what he wants."—The Voice in the Hills.

NEW CALL SIGNS

JUNE-JULY 1972

VK1JD—J. Delwood, Lawley House, Brisbane Ave. Barton, 3000.

VK1ZAZ—J. W. Carr, 34 Abernethy St., Wonthaggi, 3614.

VK1LL—C. L. Scully, 18/82 Victoria Rd., Ryde, 2112.

VK1ZB—W. J. Smith, 18 Prince St., Glenbrook, 2173.

VK2ZV—W. G. Cooley, Waldorf Private Hotel, 3 Millson Rd., Chatswood Point, 2080.

VK3AX—R. J. G. Gribble, 1/381 Belmore Rd., Riverton, 2120.

VK1BDD—R. Kilwerth, 11/85 West Kepaniwae, Manly, 2095.

VK2BPF—R. G. Gill, 5 Lower Mount St., Wentworthville, 2145.

VK2BZB—R. G. Gill, 2107.

VK1RAC—P. Dennis, Coast Amateur Radio Club, 2300-2302 St. K. Kariong, 2226.

VK1RAN—R. R. Wireless Institute of Australia, Munter Branch, 48 Valaud Cres., Highfields, 2288.

VK1RA—Orange and District Radio Society, 2288-2300 St. K. Kariong, 2226.

VK2RAS—R. L. Wireless Institute of Australia, Station Dural, Postbox: 14 Acheson St., St. Leonards, 2065.

VK2ZNU—R. Ryback, 87 Evans St., Penrith, 2700.

VK1ZND—P. Whaitate, 5/51A Forsyth St., Kingford, 2529.

VK1ZQX—R. J. Marindale, 63 Windsor Hill, 2203.

VK1ZKU—J. E. Anderson (Prof.), 78 Jakes St., Broadbeach, 2200.

VK2ZY—R. J. Smit, 6 Moore Cres., Faulconbridge, 2715.

VK2ZPZ—B. S. Scott, 21 York St., Epping, 3211.

VK2ZAS—A. M. Adams, 3 Fernleigh Gardens, 2200 Bay, 2226.

VK2ZU—C. Coles, 101 Archer St., Chatswood, 2067.

VK2ZYY—P. L. Greaves, 80 Duffy Ave., Thornleigh, 2120.

VK1SA—J. Orr, 10/12 Mooltan St., Ascot Vale, 3032.

VK1RABG—J. Mellor, Station: Princes Highway, Albion, 2715; Post: P.O. Box 65, Yarraville, 3071.

VK1BDS—T. E. H. Schoell, Lot 78, Anderson St., Boronia, 3135.

VK1BGI—O. H. R. Hobson, 18 Bentwood Cres., Frankston, 3199.

VK1BZG—2, Kurrajong Ave., Glen Waverley, 3150.

VK1BGM—L. Sampson, 478 Carson Pl., Burnley Cl., Canada, 3032.

VK3YGR—J. I. Dailwood, 7/8 Middle Rd., Maribyrnong, 3032.

VK1YHB—R. Bennett & M. Meva St., East Bentleigh, 3155.

VK2ZLC—W. R. Knight, 17 Lucas St., Newcombe, 2118.

VK2ZLZ—J. Zovi, 38 Arnold St., Princes Hill, 3054.

VK3ZTN—N. J. Melford, Old Coonara Rd., Olinda, 3780.

VK2ZWA—W. R. Deitch, 30 Cantala Dr., Doncaster, 3108.

VK5C—C. T. Younger, Station: U.S. Navcom Sdn, Exmouth, 3977; Post: P.O. Box 1, Exmouth, 3977.

VK3HBD—J. M. Mathews, Station: Drill Barge, "J. C. Mathews", Post: C.P. Mr. Middlebrook, Papua, Agencies Ltd., P.O. Box 120, Port Moresby.

VK5HO—N. K. Gustafson, Station: Sect. 41, Lot 22, St. Kilda, Post: P.O. Box 1864, Box Hill, 3128.

VK5EJ—K. V. Ford, Station: Quail St. Lee, Post: P.O. Box 1458, Lee.

VK5ZP—L. J. Fletcher, C/o. Manus High School, Louroungau.

NEW PRODUCT—50 MHz. COUNTER KIT

Decade Counting Module for Frequency Counting, Time Measurement, Event Counting, etc.

1. 30 MHz or 20 MHz counting capability.
2. Module kit consists of 7480 or 7490, 7475, 7447 and Mintron 3015F.
3. Single plane 7 seg readout.
4. Latch test, selectable ripple blanking.
5. 1000 point.
6. PC glass epoxy plug-in board.
7. Well documented application note with step-by-step assembly and hook-up instruction.

Gate Module F

1. Module consists of 7460, 7403, 7475 and 7450.
2. Adjustable reset generator.
3. Reset and strobe outputs.
4. Gate uses Schottky TTL.
5. PC glass epoxy board.
6. Application note and assembly instruction.

Input Amp. and Pulse Shaper Module

1. 1 meg ohm input impedance.
 2. 20 mV. sensitivity at 50 MHz.
 3. Diode protected PET input.
 4. Frequency response 10 Hz. to 70 MHz. plus or minus 2 dB.
 5. Glass epoxy PC board.
 6. Application note and assembly instruction.
- ALL Modules operate off plus 5 volts rail.

50 MHz. COUNTER KIT PRICE LIST
 50 MHz. Decade Module \$22.50 ea.
 20 MHz. Decade Module \$19.50 ea.
 Gate Module F \$15.75 ea.
 Input Amp. Module \$16.20 ea.
 Packing and Post 25c
 Frequency Standard and Clock Divider to be
 recommended.

INTEGRATED CIRCUITS

SN7490N	\$2.20 ea.
SN7441AN	\$2.75 ea.
SN7475N	\$2.20 ea.
SN7400N	\$1.00 ea.
SN7410N	\$1.00 ea.
SN7430N	\$1.00 ea.
SN7440N	\$1.00 ea.
SN7472N	\$1.85 ea.
SN7473N	\$2.00 ea.
SN7447N	\$3.20 ea.
LM709 Op-Amp.	\$1.50 ea.
LM305 Pos. Reg.	\$3.80 ea.
LM304 Neg. Reg.	\$4.90 ea.
TIL209 LED	\$1.50 ea.
LM380 2 watt Audio IC.	12-15v. rail,	
50K ohm input imp.	voltage gain of	
50, short circuit and overload protec-	50, short circuit and overload protec-	
tion. Price \$2.85 each	tion. Price \$2.85 each	
	Postage on ICs, 10c each.	

SPECIALS

7 seg. LED Readout, NSN4, similar to Man 1, Price 5.25 each.

RF Power Transistor, BLY89, 25 watts out at 175 MHz, rail 13.6v., balanced emitter. Only \$9.00 each, or two for \$16.00. P/P 20c.

Transistor DC-DC converter transformer, ideal for CD ignition, 12 volts input, 320 volts at 150 mA. output. Price 3.00 each, P/P 20c.

TRANSISTORS

AD140	...	\$1.00	2N3645	...	75c
2N3055	...	\$2.00	2N708	...	45c
BC109	...	60c	2N3888	...	\$1.50
BC108	...	50c	2N3819 FET	85c	
BC107	...	50c	MPF121	...	
2N3568	...	75c	TIS88	...	\$1.20

Packing and Post 10c each.

CAPACITORS—ELECTROLYTIC

1000 μ F., 100 volts	\$1.50 ea.	P/P 25c.
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Ionospheric Predictions

With Bruce Bathols,* VK3ASE

NOV. '72

Listed hereunder are the Ionospheric Predictions for November 1972, from the charts supplied by the Ionospheric Prediction Service Division.

Taking into account the predicted M.U.F. and A.R.F. these listings should provide communication between the times stated for at least 50 per cent of the month, but not all days.

All times are G.M.T.

28 MHz—

VK1/2	to W6	S.P.	0100
"	" W6	L.P.	2100, 1000-1600
"	" VE3	S.P.	1400-1600, 1900-3100
"	" VE3	L.P.	1800
"	" W6	S.P.	1400-3000
"	" W6	L.P.	0400-1100
"	" PY	S.P.	2300-1000
"	" G	S.P.	0700-1500
VK3	" UA	L.P.	0800-1100
"	" JA	S.P.	2300-3300
"	" JA	L.P.	0800-1100
"	" W1	S.P.	2300-3300
VK4	" SZ	S.P.	0600-1100, 2200-3300
"	" SZ	L.P.	1800-2300, 0800-1800
"	" W1	S.P.	1400, 1900-3400
"	" PY	S.P.	0600-1100, 2200-3300
"	" G	S.P.	0400-1500
VK5	" KH6	L.P.	0800-1100
VK6	" SU	S.P.	2400-1400
"	" W6	S.P.	2200-3300
ZL	" ZS	S.P.	0500-1000
"	" W1	S.P.	1700-3400
"	" G	S.P.	0800-1400
"	" G	L.P.	0800
14 MHz—			
VK1/2	to SP	S.P.	0300-0800, 1600-1500
"	" SP	L.P.	0900-1600
"	" VE3	S.P.	1300-2100
"	" VE3	L.P.	1300-1700, 2000-0100
"	" W6	S.P.	1500-2100, 0400-0500
"	" ZS	S.P.	1300-2100, 0800-2200
"	" ZS	L.P.	1300-2100
"	" VK6	S.P.	2300-1100
"	" G	S.P.	0800-1200
VK3	" UA	L.P.	0700-1600
"	" JA	S.P.	0500-1800, 2100-3400
"	" JA	L.P.	0700-1600
"	" W1	S.P.	1300-2000
"	" VK6	S.P.	2000-1300
VK4	" SZ	S.P.	1400-2400
"	" SZ	L.P.	0400, 0700-3000
"	" W1	S.P.	1300-2100
"	" PY	S.P.	0400-1100, 1800-3300
"	" G	S.P.	0800-1300, 2000-3300
VK5	" KH6	S.P.	0400-1500, 1700-2100
VK6	" SU	S.P.	1800-0100
"	" W6	S.P.	1600-2200, 0700
ZL	" ZS	S.P.	0300-0700
"	" W1	S.P.	1300-1800, 0200
"	" G	S.P.	0700-1800
"	" G	L.P.	1800-2300, 0100-0500
"	" G	L.P.	0700-1800
7 MHz—			
VK1/2	to W6	S.P.	0800-1600
"	" G	S.P.	1400-2000
"	" G	L.P.	0900
VK3	" JA	S.P.	0900-2000
"	" W1	S.P.	0900-1200
"	" VK6	S.P.	1800-2100
"	" VK6	L.P.	0800-1800
VK5	" SU	S.P.	1500-2300
ZL	" ZS	S.P.	1700

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MODEL N9500—0.5 watt, 6-channel intercom master unit, ideal for inter-office use. Attractive appearance, push-button operation.

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WHILE STOCKS LAST (We had 23 units)

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MASTER UNIT

MODEL 9502—5 watt, 6-channel intercom master unit, suitable for office, store-rooms, hospitals, factories and so on. Similar to Model N9500 but has 10 times the output.

USUAL TRADE PRICE **\$48.00** Plus 15% Sales Tax

WHILE STOCKS LAST (We had 77 units)

\$27.57 Plus 15%
Sales Tax

SLAVE UNIT

MODEL N9509—suitable for use with both N9500 and N9502 master units.

USUAL TRADE PRICE **\$12.93** Plus 15% Sales Tax

WHILE STOCKS LAST (We had 206 units)

\$6.40 Plus 15%
Sales Tax

MASTER UNIT Single-Channel

MODEL 9504 (used in pairs or with 9508 slave units)—key-bar operation, press-to-talk, can be locked in either talk or listen position.

USUAL TRADE PRICE **\$19.93** Plus 15% Sales Tax

WHILE STOCKS LAST (We had 41 units)

\$11.50 Plus 15%
Sales Tax

MASTER UNIT Four-Channel

MODEL 9506 (used with four only 9508 slave units)—key-bar operation, press-to-talk, can be locked in either talk or listen position. Push-button channel selection.

USUAL TRADE PRICE **\$28.87** Plus 15% Sales Tax

WHILE STOCKS LAST (We had 48 units)

\$14.67 Plus 15%
Sales Tax

SLAVE UNIT

MODEL 9508—for use with 9504 and 9506 master units. These units make attractive extension speaker installations.

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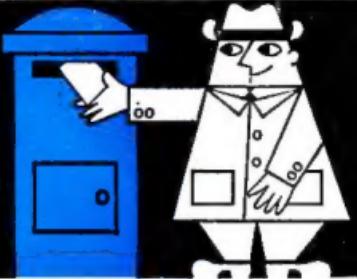
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